

## Calculating the Applied Load

The LM Guide is capable of receiving loads and moments in all directions whether they are generated by the mounting orientation and position, the location of the center of gravity of the moving object, the position of the thrust, the acceleration, or the cutting resistance.

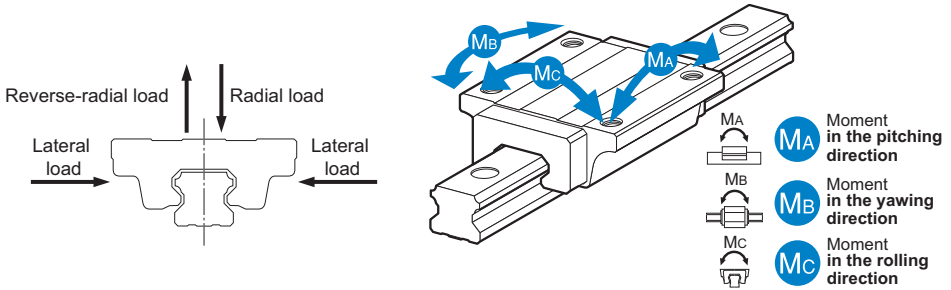


Fig. 1 Directions of the Loads Applied on the LM Guide

## Calculating an Applied Load

### Single-Axis Use

#### ● Moment Equivalence

When the space to install the LM Guide is limited, you may have to use only one LM block, or two LM blocks in close contact with each other. In such a setting, the load distribution is not uniform. As a result, an excessive load is applied in localized areas (i.e., both ends) as shown in Fig. 2. Continued use under such conditions may result in flaking in those areas, consequently shortening the service life. In such a case, calculate the actual load by multiplying the moment value by any one of the equivalent-moment factors specified in Table 1 to Table 6.

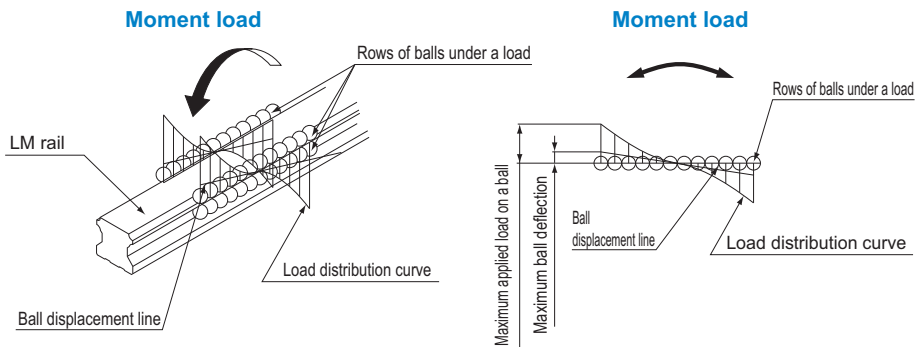


Fig. 2 Ball Load when a Moment is Applied

An equivalent-load equation applicable when a moment acts on an LM Guide is shown below.

$$P = K \cdot M$$

P : Equivalent load per LM Guide (N)

K : Equivalent moment factor

M : Applied moment (N·mm)

### ● Equivalent Factor

Since the rated load is equivalent to the permissible moment, the equivalent factor to be multiplied when equalizing the  $M_A$ ,  $M_B$ , and  $M_C$  moments to the applied load per block is obtained by dividing the rated loads in the corresponding directions.

With models other than 4-way equal load types, however, the load ratings in the 4 directions differ from each other. Therefore, the equivalent factor values for the  $M_A$  and  $M_C$  moments also differ depending on whether the direction is radial or reverse radial.

### ■ Equivalent Factors for the $M_A$ Moment

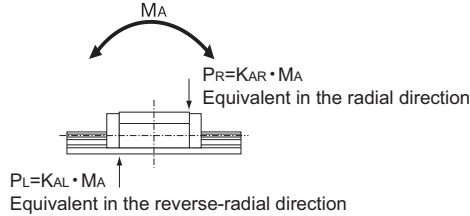


Fig. 3 Equivalent Factors for the  $M_A$  Moment

Equivalent factors for the  $M_A$  Moment

$$\left. \begin{array}{l} \text{Equivalent factor} \\ \text{in the radial direction} \end{array} \right\} K_{AR} = \frac{C_0}{M_A}$$

$$\left. \begin{array}{l} \text{Equivalent factor in the} \\ \text{reverse-radial direction} \end{array} \right\} K_{AL} = \frac{C_{0L}}{M_A}$$

$$\frac{C_0}{K_{AR} \cdot M_A} = \frac{C_{0L}}{K_{AL} \cdot M_A} = 1$$

### ■ Equivalent Factors for the $M_B$ Moment

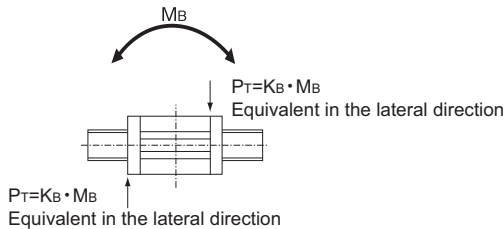


Fig. 4 Equivalent Factors for the  $M_B$  Moment

Equivalent factors for the  $M_B$  Moment

$$\left. \begin{array}{l} \text{Equivalent factor in} \\ \text{the lateral directions} \end{array} \right\} K_B = \frac{C_{0T}}{M_B}$$

$$\frac{C_{0T}}{K_B \cdot M_B} = 1$$

## ■ Equivalent Factors for the $M_c$ Moment

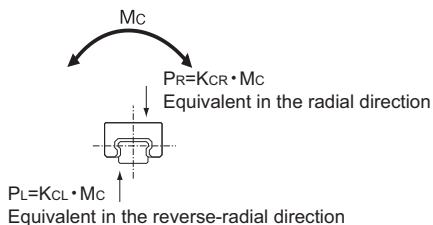


Fig. 5 Equivalent Factors for the  $M_c$  Moment

Equivalent factors for the  $M_c$  Moment

Equivalent factor  
in the radial direction  $K_{CR} = \frac{C_0}{M_c}$

Equivalent factor in the  
reverse-radial direction  $K_{CL} = \frac{C_{0L}}{M_c}$

$$\frac{C_0}{K_{CR} \cdot M_c} = \frac{C_{0L}}{K_{CL} \cdot M_c} = 1$$

$C_0$  : Basic static load rating (radial direction) (N)

$C_{0L}$  : Basic static load rating (reverse-radial direction) (N)

$C_{0T}$  : Basic static load rating (lateral direction) (N)

$P_R$  : Calculated load (radial direction) (N)

$P_L$  : Calculated load (reverse-radial direction) (N)

$P_T$  : Calculated load (lateral direction) (N)

## Selection Criteria

## Calculating the Applied Load

Table 1: Equivalent Factors (Models SHS, SSR, SVR, SVS, SHW, and SRS)

Model No.		Equivalent factor							
		K <sub>AR1</sub>	K <sub>AL1</sub>	K <sub>AR2</sub>	K <sub>AL2</sub>	K <sub>B1</sub>	K <sub>B2</sub>	K <sub>CR</sub>	K <sub>CL</sub>
SHS	15	$1.38 \times 10^{-1}$		$2.69 \times 10^{-2}$		$1.38 \times 10^{-1}$	$2.69 \times 10^{-2}$		$1.50 \times 10^{-1}$
	15L	$1.07 \times 10^{-1}$		$2.22 \times 10^{-2}$		$1.07 \times 10^{-1}$	$2.22 \times 10^{-2}$		$1.50 \times 10^{-1}$
	20	$1.15 \times 10^{-1}$		$2.18 \times 10^{-2}$		$1.15 \times 10^{-1}$	$2.18 \times 10^{-2}$		$1.06 \times 10^{-1}$
	20L	$8.85 \times 10^{-2}$		$1.79 \times 10^{-2}$		$8.85 \times 10^{-2}$	$1.79 \times 10^{-2}$		$1.06 \times 10^{-1}$
	25	$9.25 \times 10^{-2}$		$1.90 \times 10^{-2}$		$9.25 \times 10^{-2}$	$1.90 \times 10^{-2}$		$9.29 \times 10^{-2}$
	25L	$7.62 \times 10^{-2}$		$1.62 \times 10^{-2}$		$7.62 \times 10^{-2}$	$1.62 \times 10^{-2}$		$9.29 \times 10^{-2}$
	30	$8.47 \times 10^{-2}$		$1.63 \times 10^{-2}$		$8.47 \times 10^{-2}$	$1.63 \times 10^{-2}$		$7.69 \times 10^{-2}$
	30L	$6.52 \times 10^{-2}$		$1.34 \times 10^{-2}$		$6.52 \times 10^{-2}$	$1.34 \times 10^{-2}$		$7.69 \times 10^{-2}$
	35	$6.95 \times 10^{-2}$		$1.43 \times 10^{-2}$		$6.95 \times 10^{-2}$	$1.43 \times 10^{-2}$		$6.29 \times 10^{-2}$
	35L	$5.43 \times 10^{-2}$		$1.16 \times 10^{-2}$		$5.43 \times 10^{-2}$	$1.16 \times 10^{-2}$		$6.29 \times 10^{-2}$
	45	$6.13 \times 10^{-2}$		$1.24 \times 10^{-2}$		$6.13 \times 10^{-2}$	$1.24 \times 10^{-2}$		$4.69 \times 10^{-2}$
	45L	$4.79 \times 10^{-2}$		$1.02 \times 10^{-2}$		$4.79 \times 10^{-2}$	$1.02 \times 10^{-2}$		$4.69 \times 10^{-2}$
	55	$4.97 \times 10^{-2}$		$1.02 \times 10^{-2}$		$4.97 \times 10^{-2}$	$1.02 \times 10^{-2}$		$4.02 \times 10^{-2}$
	55L	$3.88 \times 10^{-2}$		$8.30 \times 10^{-3}$		$3.88 \times 10^{-2}$	$8.30 \times 10^{-3}$		$4.02 \times 10^{-2}$
	65	$3.87 \times 10^{-2}$		$7.91 \times 10^{-3}$		$3.87 \times 10^{-2}$	$7.91 \times 10^{-3}$		$3.40 \times 10^{-2}$
	65L	$3.06 \times 10^{-2}$		$6.51 \times 10^{-3}$		$3.06 \times 10^{-2}$	$6.51 \times 10^{-3}$		$3.40 \times 10^{-2}$
SSR	15XW(XTB)	$2.08 \times 10^{-1}$	$1.04 \times 10^{-1}$	$3.75 \times 10^{-2}$	$1.87 \times 10^{-2}$	$1.46 \times 10^{-1}$	$2.59 \times 10^{-2}$	$1.71 \times 10^{-1}$	$8.57 \times 10^{-2}$
	15XV(XSB)	$3.19 \times 10^{-1}$	$1.60 \times 10^{-1}$	$5.03 \times 10^{-2}$	$2.51 \times 10^{-2}$	$2.20 \times 10^{-1}$	$3.41 \times 10^{-2}$	$1.71 \times 10^{-1}$	$8.57 \times 10^{-2}$
	20XW(XTB)	$1.69 \times 10^{-1}$	$8.46 \times 10^{-2}$	$3.23 \times 10^{-2}$	$1.62 \times 10^{-2}$	$1.19 \times 10^{-1}$	$2.25 \times 10^{-2}$	$1.29 \times 10^{-1}$	$6.44 \times 10^{-2}$
	20XV(XSB)	$2.75 \times 10^{-1}$	$1.37 \times 10^{-1}$	$4.28 \times 10^{-2}$	$2.14 \times 10^{-2}$	$1.89 \times 10^{-1}$	$2.89 \times 10^{-2}$	$1.29 \times 10^{-1}$	$6.44 \times 10^{-2}$
	25XW(XTB)	$1.41 \times 10^{-1}$	$7.05 \times 10^{-2}$	$2.56 \times 10^{-2}$	$1.28 \times 10^{-2}$	$9.86 \times 10^{-2}$	$1.77 \times 10^{-2}$	$1.10 \times 10^{-1}$	$5.51 \times 10^{-2}$
	25XV(XSB)	$2.15 \times 10^{-1}$	$1.08 \times 10^{-1}$	$3.40 \times 10^{-2}$	$1.70 \times 10^{-2}$	$1.48 \times 10^{-1}$	$2.31 \times 10^{-2}$	$1.10 \times 10^{-1}$	$5.51 \times 10^{-2}$
	30XW(XTB)	$1.18 \times 10^{-1}$	$5.91 \times 10^{-2}$	$2.19 \times 10^{-2}$	$1.10 \times 10^{-2}$	$8.26 \times 10^{-2}$	$1.52 \times 10^{-2}$	$9.22 \times 10^{-2}$	$4.61 \times 10^{-2}$
	30XV(XSB)	$1.85 \times 10^{-1}$	$9.24 \times 10^{-2}$	$4.69 \times 10^{-2}$	$2.34 \times 10^{-2}$	$1.27 \times 10^{-1}$	$3.19 \times 10^{-2}$	$9.16 \times 10^{-2}$	$4.58 \times 10^{-2}$
	35XW(XTB)	$1.01 \times 10^{-1}$	$5.03 \times 10^{-2}$	$1.92 \times 10^{-2}$	$9.60 \times 10^{-3}$	$7.04 \times 10^{-2}$	$1.33 \times 10^{-2}$	$7.64 \times 10^{-2}$	$3.82 \times 10^{-2}$
	35XV(XSB)	$1.58 \times 10^{-1}$	$7.91 \times 10^{-2}$	$4.04 \times 10^{-2}$	$2.02 \times 10^{-2}$	$1.09 \times 10^{-1}$	$2.75 \times 10^{-2}$	$7.59 \times 10^{-2}$	$3.80 \times 10^{-2}$
SVR	25	$1.13 \times 10^{-1}$	$7.28 \times 10^{-2}$	$2.25 \times 10^{-2}$	$1.45 \times 10^{-2}$	$7.14 \times 10^{-2}$	$1.43 \times 10^{-2}$	$9.59 \times 10^{-2}$	$6.17 \times 10^{-2}$
	25L	$9.14 \times 10^{-2}$	$5.88 \times 10^{-2}$	$1.85 \times 10^{-2}$	$1.19 \times 10^{-2}$	$5.80 \times 10^{-2}$	$1.17 \times 10^{-2}$	$9.59 \times 10^{-2}$	$6.17 \times 10^{-2}$
	30	$1.01 \times 10^{-1}$	$6.50 \times 10^{-2}$	$1.89 \times 10^{-2}$	$1.21 \times 10^{-2}$	$6.36 \times 10^{-2}$	$1.19 \times 10^{-2}$	$8.45 \times 10^{-2}$	$5.43 \times 10^{-2}$
	30L	$7.56 \times 10^{-2}$	$4.86 \times 10^{-2}$	$1.57 \times 10^{-2}$	$1.01 \times 10^{-2}$	$4.79 \times 10^{-2}$	$1.00 \times 10^{-2}$	$8.45 \times 10^{-2}$	$5.43 \times 10^{-2}$
	35	$9.19 \times 10^{-2}$	$5.91 \times 10^{-2}$	$1.68 \times 10^{-2}$	$1.08 \times 10^{-2}$	$5.77 \times 10^{-2}$	$1.06 \times 10^{-2}$	$7.08 \times 10^{-2}$	$4.55 \times 10^{-2}$
	35L	$6.80 \times 10^{-2}$	$4.37 \times 10^{-2}$	$1.39 \times 10^{-2}$	$8.97 \times 10^{-3}$	$4.31 \times 10^{-2}$	$8.86 \times 10^{-3}$	$7.08 \times 10^{-2}$	$4.55 \times 10^{-2}$
	45	$6.73 \times 10^{-2}$	$4.33 \times 10^{-2}$	$1.35 \times 10^{-2}$	$8.71 \times 10^{-3}$	$4.25 \times 10^{-2}$	$8.59 \times 10^{-3}$	$5.32 \times 10^{-2}$	$3.42 \times 10^{-2}$
	45L	$5.40 \times 10^{-2}$	$3.47 \times 10^{-2}$	$1.10 \times 10^{-2}$	$7.09 \times 10^{-3}$	$3.41 \times 10^{-2}$	$6.97 \times 10^{-3}$	$5.30 \times 10^{-2}$	$3.41 \times 10^{-2}$
	55	$5.89 \times 10^{-2}$	$3.79 \times 10^{-2}$	$1.14 \times 10^{-2}$	$7.35 \times 10^{-3}$	$3.72 \times 10^{-2}$	$7.24 \times 10^{-3}$	$4.63 \times 10^{-2}$	$2.98 \times 10^{-2}$
	55L	$4.55 \times 10^{-2}$	$2.92 \times 10^{-2}$	$9.45 \times 10^{-3}$	$6.08 \times 10^{-3}$	$2.89 \times 10^{-2}$	$6.02 \times 10^{-3}$	$4.63 \times 10^{-2}$	$2.98 \times 10^{-2}$
	65	$4.85 \times 10^{-2}$	$3.12 \times 10^{-2}$	$1.01 \times 10^{-2}$	$6.48 \times 10^{-3}$	$3.06 \times 10^{-2}$	$6.40 \times 10^{-3}$	$3.91 \times 10^{-2}$	$2.51 \times 10^{-2}$
65L	$3.58 \times 10^{-2}$	$2.30 \times 10^{-2}$	$7.73 \times 10^{-3}$	$4.97 \times 10^{-3}$	$2.28 \times 10^{-2}$	$4.93 \times 10^{-3}$	$3.91 \times 10^{-2}$	$2.51 \times 10^{-2}$	

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
SVS	25	$1.09 \times 10^{-1}$	$9.14 \times 10^{-2}$	$2.17 \times 10^{-2}$	$1.82 \times 10^{-2}$	$1.00 \times 10^{-1}$	$2.00 \times 10^{-2}$	$9.95 \times 10^{-2}$	$8.35 \times 10^{-2}$
	25L	$8.82 \times 10^{-2}$	$7.40 \times 10^{-2}$	$1.78 \times 10^{-2}$	$1.50 \times 10^{-2}$	$8.13 \times 10^{-2}$	$1.64 \times 10^{-2}$	$9.95 \times 10^{-2}$	$8.35 \times 10^{-2}$
	30	$9.71 \times 10^{-2}$	$8.15 \times 10^{-2}$	$1.82 \times 10^{-2}$	$1.52 \times 10^{-2}$	$8.95 \times 10^{-2}$	$1.67 \times 10^{-2}$	$8.78 \times 10^{-2}$	$7.37 \times 10^{-2}$
	30L	$7.29 \times 10^{-2}$	$6.11 \times 10^{-2}$	$1.51 \times 10^{-2}$	$1.27 \times 10^{-2}$	$6.72 \times 10^{-2}$	$1.39 \times 10^{-2}$	$8.78 \times 10^{-2}$	$7.37 \times 10^{-2}$
	35	$8.84 \times 10^{-2}$	$7.42 \times 10^{-2}$	$1.61 \times 10^{-2}$	$1.35 \times 10^{-2}$	$8.14 \times 10^{-2}$	$1.48 \times 10^{-2}$	$7.36 \times 10^{-2}$	$6.17 \times 10^{-2}$
	35L	$6.56 \times 10^{-2}$	$5.50 \times 10^{-2}$	$1.34 \times 10^{-2}$	$1.13 \times 10^{-2}$	$6.04 \times 10^{-2}$	$1.24 \times 10^{-2}$	$7.36 \times 10^{-2}$	$6.17 \times 10^{-2}$
	45	$6.48 \times 10^{-2}$	$5.44 \times 10^{-2}$	$1.30 \times 10^{-2}$	$1.09 \times 10^{-2}$	$5.98 \times 10^{-2}$	$1.20 \times 10^{-2}$	$5.45 \times 10^{-2}$	$4.57 \times 10^{-2}$
	45L	$5.22 \times 10^{-2}$	$4.38 \times 10^{-2}$	$1.07 \times 10^{-2}$	$8.94 \times 10^{-3}$	$4.81 \times 10^{-2}$	$9.81 \times 10^{-3}$	$5.44 \times 10^{-2}$	$4.56 \times 10^{-2}$
	55	$5.67 \times 10^{-2}$	$4.76 \times 10^{-2}$	$1.10 \times 10^{-2}$	$9.24 \times 10^{-3}$	$5.23 \times 10^{-2}$	$1.01 \times 10^{-2}$	$4.78 \times 10^{-2}$	$4.01 \times 10^{-2}$
	55L	$4.39 \times 10^{-2}$	$3.68 \times 10^{-2}$	$9.12 \times 10^{-3}$	$7.65 \times 10^{-3}$	$4.05 \times 10^{-2}$	$8.40 \times 10^{-3}$	$4.78 \times 10^{-2}$	$4.01 \times 10^{-2}$
	65	$4.67 \times 10^{-2}$	$3.92 \times 10^{-2}$	$9.72 \times 10^{-3}$	$8.15 \times 10^{-3}$	$4.30 \times 10^{-2}$	$8.95 \times 10^{-3}$	$4.04 \times 10^{-2}$	$3.39 \times 10^{-2}$
	65L	$3.46 \times 10^{-2}$	$2.90 \times 10^{-2}$	$7.46 \times 10^{-3}$	$6.26 \times 10^{-3}$	$3.19 \times 10^{-2}$	$6.88 \times 10^{-3}$	$4.04 \times 10^{-2}$	$3.39 \times 10^{-2}$
SHW	12	$2.48 \times 10^{-1}$		$4.69 \times 10^{-2}$		$2.48 \times 10^{-1}$	$4.69 \times 10^{-2}$	$1.40 \times 10^{-1}$	
	12HR	$1.70 \times 10^{-1}$		$3.52 \times 10^{-2}$		$1.70 \times 10^{-1}$	$3.52 \times 10^{-2}$	$1.40 \times 10^{-1}$	
	14	$1.92 \times 10^{-1}$		$3.80 \times 10^{-2}$		$1.92 \times 10^{-1}$	$3.80 \times 10^{-2}$	$9.93 \times 10^{-2}$	
	17	$1.72 \times 10^{-1}$		$3.41 \times 10^{-2}$		$1.72 \times 10^{-1}$	$3.41 \times 10^{-2}$	$6.21 \times 10^{-2}$	
	21	$1.59 \times 10^{-1}$		$2.95 \times 10^{-2}$		$1.59 \times 10^{-1}$	$2.95 \times 10^{-2}$	$5.57 \times 10^{-2}$	
	27	$1.21 \times 10^{-1}$		$2.39 \times 10^{-2}$		$1.21 \times 10^{-1}$	$2.39 \times 10^{-2}$	$4.99 \times 10^{-2}$	
	35	$8.15 \times 10^{-2}$		$1.64 \times 10^{-2}$		$8.15 \times 10^{-2}$	$1.64 \times 10^{-2}$	$3.02 \times 10^{-2}$	
50	$6.22 \times 10^{-2}$		$1.24 \times 10^{-2}$		$6.22 \times 10^{-2}$	$1.24 \times 10^{-2}$	$2.30 \times 10^{-2}$		
SRS	5M	$6.33 \times 10^{-1}$		$9.20 \times 10^{-2}$		$6.45 \times 10^{-1}$	$9.30 \times 10^{-2}$	$3.85 \times 10^{-1}$	
	5GM	$6.71 \times 10^{-1}$		$9.15 \times 10^{-2}$		$6.66 \times 10^{-1}$	$9.08 \times 10^{-2}$	$3.85 \times 10^{-1}$	
	5N	$5.23 \times 10^{-1}$		$7.87 \times 10^{-2}$		$5.32 \times 10^{-1}$	$7.99 \times 10^{-2}$	$3.86 \times 10^{-1}$	
	5GN	$5.25 \times 10^{-1}$		$7.97 \times 10^{-2}$		$5.33 \times 10^{-1}$	$8.12 \times 10^{-2}$	$3.84 \times 10^{-1}$	
	5WM	$4.48 \times 10^{-1}$		$7.30 \times 10^{-2}$		$4.56 \times 10^{-1}$	$7.40 \times 10^{-2}$	$1.96 \times 10^{-1}$	
	5WGM	$4.58 \times 10^{-1}$		$7.39 \times 10^{-2}$		$4.54 \times 10^{-1}$	$7.34 \times 10^{-2}$	$1.96 \times 10^{-1}$	
	5WN	$3.31 \times 10^{-1}$		$5.93 \times 10^{-2}$		$3.36 \times 10^{-1}$	$6.02 \times 10^{-2}$	$1.96 \times 10^{-1}$	
	5WGN	$3.31 \times 10^{-1}$		$5.97 \times 10^{-2}$		$3.35 \times 10^{-1}$	$6.05 \times 10^{-2}$	$1.96 \times 10^{-1}$	
	7S	$6.03 \times 10^{-1}$		$7.65 \times 10^{-2}$		$6.27 \times 10^{-1}$	$7.91 \times 10^{-2}$	$2.58 \times 10^{-1}$	
	7GS	$5.92 \times 10^{-1}$		$7.89 \times 10^{-2}$		$6.14 \times 10^{-1}$	$8.17 \times 10^{-2}$	$2.58 \times 10^{-1}$	
	7M	$4.19 \times 10^{-1}$		$6.76 \times 10^{-2}$		$4.18 \times 10^{-1}$	$6.94 \times 10^{-2}$	$2.58 \times 10^{-1}$	
	7GM	$4.27 \times 10^{-1}$		$6.04 \times 10^{-2}$		$4.43 \times 10^{-1}$	$6.23 \times 10^{-2}$	$2.34 \times 10^{-1}$	
	7N	$2.97 \times 10^{-1}$		$5.35 \times 10^{-2}$		$3.07 \times 10^{-1}$	$5.50 \times 10^{-2}$	$2.58 \times 10^{-1}$	
	7GN	$3.11 \times 10^{-1}$		$5.35 \times 10^{-2}$		$3.20 \times 10^{-1}$	$5.51 \times 10^{-2}$	$2.58 \times 10^{-1}$	
	7WS	$4.67 \times 10^{-1}$		$6.89 \times 10^{-2}$		$4.84 \times 10^{-1}$	$7.08 \times 10^{-2}$	$1.36 \times 10^{-1}$	
	7WGS	$5.23 \times 10^{-1}$		$6.75 \times 10^{-2}$		$5.43 \times 10^{-1}$	$6.95 \times 10^{-2}$	$1.36 \times 10^{-1}$	
	7WM	$3.01 \times 10^{-1}$		$5.32 \times 10^{-2}$		$3.00 \times 10^{-1}$	$5.46 \times 10^{-2}$	$1.36 \times 10^{-1}$	
7WGM	$2.83 \times 10^{-1}$		$4.87 \times 10^{-2}$		$2.93 \times 10^{-1}$	$5.02 \times 10^{-2}$	$1.24 \times 10^{-1}$		
7WN	$2.19 \times 10^{-1}$		$4.16 \times 10^{-2}$		$2.24 \times 10^{-1}$	$4.28 \times 10^{-2}$	$1.36 \times 10^{-1}$		
7WGN	$2.20 \times 10^{-1}$		$4.17 \times 10^{-2}$		$2.27 \times 10^{-1}$	$4.31 \times 10^{-2}$	$1.36 \times 10^{-1}$		

$K_{AR1}$  : Equivalent factor in the  $M_r$  radial direction when one LM block is used  
 $K_{AL1}$  : Equivalent factor in the  $M_r$  reverse-radial direction when one LM block is used  
 $K_{AR2}$  : Equivalent factor in the  $M_A$  radial direction when two LM blocks are used in close contact with each other  
 $K_{AL2}$  : Equivalent factor in the  $M_A$  reverse-radial direction when two LM blocks are used in close contact with each other

$K_{B1}$  :  $M_s$  Equivalent factor when one LM block is used  
 $K_{B2}$  :  $M_s$  Equivalent factor when two LM blocks are used in close contact with each other  
 $K_{CR}$  : Equivalent factor in the  $M_c$  radial direction  
 $K_{CL}$  : Equivalent factor in the  $M_c$  reverse-radial direction

## Selection Criteria

## Calculating the Applied Load

Table 2: Equivalent Factors (Models SRS, SCR, EPF, and HSR)

Model No.		Equivalent factor							
		K <sub>AR1</sub>	K <sub>AL1</sub>	K <sub>AR2</sub>	K <sub>AL2</sub>	K <sub>B1</sub>	K <sub>B2</sub>	K <sub>CR</sub>	K <sub>CL</sub>
SRS	9XS	4.86 × 10 <sup>-1</sup>		6.89 × 10 <sup>-2</sup>		5.04 × 10 <sup>-1</sup>	7.11 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>
	9XGS	5.37 × 10 <sup>-1</sup>		6.77 × 10 <sup>-2</sup>		5.57 × 10 <sup>-1</sup>	7.00 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>
	9XM	2.95 × 10 <sup>-1</sup>		5.27 × 10 <sup>-2</sup>		3.06 × 10 <sup>-1</sup>	5.43 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>
	9XGM	3.10 × 10 <sup>-1</sup>		5.28 × 10 <sup>-2</sup>		3.19 × 10 <sup>-1</sup>	5.44 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>
	9XN	2.13 × 10 <sup>-1</sup>		4.12 × 10 <sup>-2</sup>		2.19 × 10 <sup>-1</sup>	4.23 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>
	9XGN	2.18 × 10 <sup>-1</sup>		4.14 × 10 <sup>-2</sup>		2.24 × 10 <sup>-1</sup>	4.27 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>
	9WS	4.10 × 10 <sup>-1</sup>		5.73 × 10 <sup>-2</sup>		4.25 × 10 <sup>-1</sup>	5.63 × 10 <sup>-2</sup>		1.06 × 10 <sup>-1</sup>
	9WGS	4.16 × 10 <sup>-1</sup>		5.80 × 10 <sup>-2</sup>		4.30 × 10 <sup>-1</sup>	5.98 × 10 <sup>-2</sup>		1.06 × 10 <sup>-1</sup>
	9WM	2.37 × 10 <sup>-1</sup>		4.25 × 10 <sup>-2</sup>		2.44 × 10 <sup>-1</sup>	4.37 × 10 <sup>-2</sup>		1.06 × 10 <sup>-1</sup>
	9WGM	2.41 × 10 <sup>-1</sup>		4.80 × 10 <sup>-2</sup>		2.41 × 10 <sup>-1</sup>	4.13 × 10 <sup>-2</sup>		1.06 × 10 <sup>-1</sup>
	9WN	1.74 × 10 <sup>-1</sup>		3.35 × 10 <sup>-2</sup>		1.78 × 10 <sup>-1</sup>	3.44 × 10 <sup>-2</sup>		1.06 × 10 <sup>-1</sup>
	9WGN	1.75 × 10 <sup>-1</sup>		3.38 × 10 <sup>-2</sup>		1.73 × 10 <sup>-1</sup>	3.32 × 10 <sup>-2</sup>		1.06 × 10 <sup>-1</sup>
	12S	4.55 × 10 <sup>-1</sup>		5.60 × 10 <sup>-2</sup>		4.55 × 10 <sup>-1</sup>	5.60 × 10 <sup>-2</sup>		1.52 × 10 <sup>-1</sup>
	12GS	5.04 × 10 <sup>-1</sup>		5.51 × 10 <sup>-2</sup>		5.04 × 10 <sup>-1</sup>	5.51 × 10 <sup>-2</sup>		1.52 × 10 <sup>-1</sup>
	12M	2.94 × 10 <sup>-1</sup>		4.50 × 10 <sup>-2</sup>		2.94 × 10 <sup>-1</sup>	4.50 × 10 <sup>-2</sup>		1.53 × 10 <sup>-1</sup>
	12GM	2.93 × 10 <sup>-1</sup>		4.49 × 10 <sup>-2</sup>		2.93 × 10 <sup>-1</sup>	4.49 × 10 <sup>-2</sup>		1.53 × 10 <sup>-1</sup>
	12N	1.86 × 10 <sup>-1</sup>		3.51 × 10 <sup>-2</sup>		1.86 × 10 <sup>-1</sup>	3.51 × 10 <sup>-2</sup>		1.53 × 10 <sup>-1</sup>
	12GN	1.96 × 10 <sup>-1</sup>		3.50 × 10 <sup>-2</sup>		1.96 × 10 <sup>-1</sup>	3.50 × 10 <sup>-2</sup>		1.53 × 10 <sup>-1</sup>
	12WS	3.22 × 10 <sup>-1</sup>		5.00 × 10 <sup>-2</sup>		3.22 × 10 <sup>-1</sup>	5.00 × 10 <sup>-2</sup>		7.97 × 10 <sup>-2</sup>
	12WGS	3.32 × 10 <sup>-1</sup>		5.07 × 10 <sup>-2</sup>		3.32 × 10 <sup>-1</sup>	5.07 × 10 <sup>-2</sup>		7.97 × 10 <sup>-2</sup>
	12WM	2.00 × 10 <sup>-1</sup>		3.69 × 10 <sup>-2</sup>		2.00 × 10 <sup>-1</sup>	3.69 × 10 <sup>-2</sup>		7.97 × 10 <sup>-2</sup>
	12WGM	2.07 × 10 <sup>-1</sup>		3.64 × 10 <sup>-2</sup>		2.07 × 10 <sup>-1</sup>	3.64 × 10 <sup>-2</sup>		7.96 × 10 <sup>-2</sup>
	12WN	1.44 × 10 <sup>-1</sup>		2.83 × 10 <sup>-2</sup>		1.44 × 10 <sup>-1</sup>	2.83 × 10 <sup>-2</sup>		7.97 × 10 <sup>-2</sup>
	12WGN	1.46 × 10 <sup>-1</sup>		2.85 × 10 <sup>-2</sup>		1.46 × 10 <sup>-1</sup>	2.85 × 10 <sup>-2</sup>		7.95 × 10 <sup>-2</sup>
	15S	3.56 × 10 <sup>-1</sup>		4.38 × 10 <sup>-2</sup>		3.56 × 10 <sup>-1</sup>	4.38 × 10 <sup>-2</sup>		1.41 × 10 <sup>-1</sup>
	15GS	3.37 × 10 <sup>-1</sup>		4.57 × 10 <sup>-2</sup>		3.37 × 10 <sup>-1</sup>	4.57 × 10 <sup>-2</sup>		1.41 × 10 <sup>-1</sup>
	15M	2.17 × 10 <sup>-1</sup>		3.69 × 10 <sup>-2</sup>		2.17 × 10 <sup>-1</sup>	3.69 × 10 <sup>-2</sup>		1.41 × 10 <sup>-1</sup>
	15GM	2.31 × 10 <sup>-1</sup>		3.61 × 10 <sup>-2</sup>		2.31 × 10 <sup>-1</sup>	3.61 × 10 <sup>-2</sup>		1.41 × 10 <sup>-1</sup>
	15N	1.43 × 10 <sup>-1</sup>		2.73 × 10 <sup>-2</sup>		1.43 × 10 <sup>-1</sup>	2.73 × 10 <sup>-2</sup>		1.41 × 10 <sup>-1</sup>
	15GN	1.45 × 10 <sup>-1</sup>		2.75 × 10 <sup>-2</sup>		1.45 × 10 <sup>-1</sup>	2.75 × 10 <sup>-2</sup>		1.41 × 10 <sup>-1</sup>
	15WS	2.34 × 10 <sup>-1</sup>		3.76 × 10 <sup>-2</sup>		2.34 × 10 <sup>-1</sup>	3.76 × 10 <sup>-2</sup>		4.83 × 10 <sup>-2</sup>
	15WGS	2.34 × 10 <sup>-1</sup>		3.81 × 10 <sup>-2</sup>		2.34 × 10 <sup>-1</sup>	3.81 × 10 <sup>-2</sup>		4.84 × 10 <sup>-2</sup>
	15WM	1.67 × 10 <sup>-1</sup>		2.94 × 10 <sup>-2</sup>		1.67 × 10 <sup>-1</sup>	2.94 × 10 <sup>-2</sup>		4.83 × 10 <sup>-2</sup>
	15WGM	1.63 × 10 <sup>-1</sup>		2.93 × 10 <sup>-2</sup>		1.63 × 10 <sup>-1</sup>	2.93 × 10 <sup>-2</sup>		4.83 × 10 <sup>-2</sup>
	15WN	1.13 × 10 <sup>-1</sup>		2.27 × 10 <sup>-2</sup>		1.13 × 10 <sup>-1</sup>	2.27 × 10 <sup>-2</sup>		4.83 × 10 <sup>-2</sup>
	15WGN	1.15 × 10 <sup>-1</sup>		2.28 × 10 <sup>-2</sup>		1.15 × 10 <sup>-1</sup>	2.28 × 10 <sup>-2</sup>		4.83 × 10 <sup>-2</sup>
	20M	1.80 × 10 <sup>-1</sup>		3.30 × 10 <sup>-2</sup>		1.86 × 10 <sup>-1</sup>	3.41 × 10 <sup>-2</sup>		9.34 × 10 <sup>-2</sup>
	20GM	2.10 × 10 <sup>-1</sup>		3.88 × 10 <sup>-2</sup>		2.10 × 10 <sup>-1</sup>	3.87 × 10 <sup>-2</sup>		1.03 × 10 <sup>-1</sup>
	25M	1.14 × 10 <sup>-1</sup>		2.17 × 10 <sup>-2</sup>		1.14 × 10 <sup>-1</sup>	2.17 × 10 <sup>-2</sup>		8.13 × 10 <sup>-2</sup>
	25GM	1.23 × 10 <sup>-1</sup>		2.32 × 10 <sup>-2</sup>		1.23 × 10 <sup>-1</sup>	2.32 × 10 <sup>-2</sup>		8.75 × 10 <sup>-2</sup>

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
SCR	15S	$1.38 \times 10^{-1}$		$2.69 \times 10^{-2}$		$1.38 \times 10^{-1}$		—	
	20S	$1.15 \times 10^{-1}$		$2.18 \times 10^{-2}$		$1.15 \times 10^{-1}$		—	
	20	$8.85 \times 10^{-2}$		$1.79 \times 10^{-2}$		$8.85 \times 10^{-2}$		—	
	25	$9.25 \times 10^{-2}$		$1.90 \times 10^{-2}$		$9.25 \times 10^{-2}$	$1.90 \times 10^{-2}$	—	
	30	$8.47 \times 10^{-2}$		$1.63 \times 10^{-2}$		$8.47 \times 10^{-2}$	$1.63 \times 10^{-2}$	—	
	35	$6.95 \times 10^{-2}$		$1.43 \times 10^{-2}$		$6.95 \times 10^{-2}$	$1.43 \times 10^{-2}$	—	
	45	$6.13 \times 10^{-2}$		$1.24 \times 10^{-2}$		$6.13 \times 10^{-2}$	$1.24 \times 10^{-2}$	—	
	65	$3.87 \times 10^{-2}$		$7.91 \times 10^{-3}$		$3.87 \times 10^{-2}$	$7.91 \times 10^{-3}$	—	
EPF	7M	$3.55 \times 10^{-1}$		—		$3.55 \times 10^{-1}$		$2.86 \times 10^{-1}$	
	9M	$3.10 \times 10^{-1}$		—		$3.10 \times 10^{-1}$		$2.22 \times 10^{-1}$	
	12M	$2.68 \times 10^{-1}$		—		$2.68 \times 10^{-1}$		$1.67 \times 10^{-1}$	
	15M	$2.00 \times 10^{-1}$		—		$2.00 \times 10^{-1}$		$1.34 \times 10^{-1}$	
HSR	8	$4.39 \times 10^{-1}$		$6.75 \times 10^{-2}$		$4.39 \times 10^{-1}$	$6.75 \times 10^{-2}$	$2.97 \times 10^{-1}$	
	10	$3.09 \times 10^{-1}$		$5.33 \times 10^{-2}$		$3.09 \times 10^{-1}$	$5.33 \times 10^{-2}$	$2.35 \times 10^{-1}$	
	12	$2.08 \times 10^{-1}$		$3.74 \times 10^{-2}$		$2.08 \times 10^{-1}$	$3.74 \times 10^{-2}$	$1.91 \times 10^{-1}$	
	15	$1.66 \times 10^{-1}$		$2.98 \times 10^{-2}$		$1.66 \times 10^{-1}$	$2.98 \times 10^{-2}$	$1.57 \times 10^{-1}$	
	15L	$1.18 \times 10^{-1}$		$2.33 \times 10^{-2}$		$1.18 \times 10^{-1}$	$2.33 \times 10^{-2}$	$1.57 \times 10^{-1}$	
	20	$1.26 \times 10^{-1}$		$2.28 \times 10^{-2}$		$1.26 \times 10^{-1}$	$2.28 \times 10^{-2}$	$1.17 \times 10^{-1}$	
	20L	$9.88 \times 10^{-2}$		$1.92 \times 10^{-2}$		$9.88 \times 10^{-2}$	$1.92 \times 10^{-2}$	$1.17 \times 10^{-1}$	
	25	$1.12 \times 10^{-1}$		$2.02 \times 10^{-2}$		$1.12 \times 10^{-1}$	$2.02 \times 10^{-2}$	$9.96 \times 10^{-2}$	
	25L	$8.23 \times 10^{-2}$		$1.70 \times 10^{-2}$		$8.23 \times 10^{-2}$	$1.70 \times 10^{-2}$	$9.96 \times 10^{-2}$	
	30	$8.97 \times 10^{-2}$		$1.73 \times 10^{-2}$		$8.97 \times 10^{-2}$	$1.73 \times 10^{-2}$	$8.24 \times 10^{-2}$	
	30L	$7.05 \times 10^{-2}$		$1.44 \times 10^{-2}$		$7.05 \times 10^{-2}$	$1.44 \times 10^{-2}$	$8.24 \times 10^{-2}$	
	35	$7.85 \times 10^{-2}$		$1.56 \times 10^{-2}$		$7.85 \times 10^{-2}$	$1.56 \times 10^{-2}$	$6.69 \times 10^{-2}$	
	35L	$6.17 \times 10^{-2}$		$1.29 \times 10^{-2}$		$6.17 \times 10^{-2}$	$1.29 \times 10^{-2}$	$6.69 \times 10^{-2}$	
	45	$6.73 \times 10^{-2}$		$1.21 \times 10^{-2}$		$6.73 \times 10^{-2}$	$1.21 \times 10^{-2}$	$5.20 \times 10^{-2}$	
	45L	$5.22 \times 10^{-2}$		$1.01 \times 10^{-2}$		$5.22 \times 10^{-2}$	$1.01 \times 10^{-2}$	$5.20 \times 10^{-2}$	
	55	$5.61 \times 10^{-2}$		$1.03 \times 10^{-2}$		$5.61 \times 10^{-2}$	$1.03 \times 10^{-2}$	$4.26 \times 10^{-2}$	
	55L	$4.35 \times 10^{-2}$		$8.56 \times 10^{-3}$		$4.35 \times 10^{-2}$	$8.56 \times 10^{-3}$	$4.26 \times 10^{-2}$	
	65	$4.49 \times 10^{-2}$		$9.13 \times 10^{-3}$		$4.49 \times 10^{-2}$	$9.13 \times 10^{-3}$	$3.68 \times 10^{-2}$	
	65L	$3.29 \times 10^{-2}$		$7.08 \times 10^{-3}$		$3.29 \times 10^{-2}$	$7.08 \times 10^{-3}$	$3.68 \times 10^{-2}$	
	85	$3.49 \times 10^{-2}$		$6.94 \times 10^{-3}$		$3.49 \times 10^{-2}$	$6.94 \times 10^{-3}$	$2.78 \times 10^{-2}$	
	85L	$2.74 \times 10^{-2}$		$5.72 \times 10^{-3}$		$2.74 \times 10^{-2}$	$5.72 \times 10^{-3}$	$2.78 \times 10^{-2}$	
	100	$2.61 \times 10^{-2}$		$5.16 \times 10^{-3}$		$2.61 \times 10^{-2}$	$5.16 \times 10^{-3}$	$2.24 \times 10^{-2}$	
	120	$2.37 \times 10^{-2}$		$4.72 \times 10^{-3}$		$2.37 \times 10^{-2}$	$4.72 \times 10^{-3}$	$1.96 \times 10^{-2}$	
150	$2.17 \times 10^{-2}$		$4.35 \times 10^{-3}$		$2.17 \times 10^{-2}$	$4.35 \times 10^{-3}$	$1.61 \times 10^{-2}$		
15M2A	$1.65 \times 10^{-1}$		$2.89 \times 10^{-2}$		$1.65 \times 10^{-1}$	$2.89 \times 10^{-2}$	$1.86 \times 10^{-1}$		
20M2A	$1.23 \times 10^{-1}$		$2.23 \times 10^{-2}$		$1.23 \times 10^{-1}$	$2.23 \times 10^{-2}$	$1.34 \times 10^{-1}$		
25M2A	$1.10 \times 10^{-1}$		$1.98 \times 10^{-2}$		$1.10 \times 10^{-1}$	$1.98 \times 10^{-2}$	$1.14 \times 10^{-1}$		

$K_{AR1}$  : Equivalent factor in the  $M_A$  radial direction when one LM block is used

$K_{AL1}$  : Equivalent factor in the  $M_A$  reverse-radial direction when one LM block is used

$K_{AR2}$  : Equivalent factor in the  $M_A$  radial direction when two LM blocks are used in close contact with each other

$K_{AL2}$  : Equivalent factor in the  $M_A$  reverse-radial direction when two LM blocks are used in close contact with each other

$K_{B1}$  :  $M_B$  Equivalent factor when one LM block is used

$K_{B2}$  :  $M_B$  Equivalent factor when two LM blocks are used in close contact with each other

$K_{CR}$  : Equivalent factor in the  $M_C$  radial direction

$K_{CL}$  : Equivalent factor in the  $M_C$  reverse-radial direction

## Selection Criteria

## Calculating the Applied Load

Table 3: Equivalent Factors (Models SR, NR-X, and NR)

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
SR	15W (TB)	$2.08 \times 10^{-1}$	$1.04 \times 10^{-1}$	$3.72 \times 10^{-2}$	$1.86 \times 10^{-2}$	$1.46 \times 10^{-1}$	$2.57 \times 10^{-2}$	$1.69 \times 10^{-1}$	$8.43 \times 10^{-2}$
	15V (SB)	$3.40 \times 10^{-1}$	$1.70 \times 10^{-1}$	$5.00 \times 10^{-2}$	$2.50 \times 10^{-2}$	$2.34 \times 10^{-1}$	$3.37 \times 10^{-2}$	$1.69 \times 10^{-1}$	$8.43 \times 10^{-2}$
	20W (TB)	$1.71 \times 10^{-1}$	$8.56 \times 10^{-2}$	$3.23 \times 10^{-2}$	$1.61 \times 10^{-2}$	$1.20 \times 10^{-1}$	$2.24 \times 10^{-2}$	$1.28 \times 10^{-1}$	$6.40 \times 10^{-2}$
	20V (SB)	$2.69 \times 10^{-1}$	$1.34 \times 10^{-1}$	$4.34 \times 10^{-2}$	$2.17 \times 10^{-2}$	$1.86 \times 10^{-1}$	$2.95 \times 10^{-2}$	$1.28 \times 10^{-1}$	$6.39 \times 10^{-2}$
	25W (TB)	$1.37 \times 10^{-1}$	$6.85 \times 10^{-2}$	$2.57 \times 10^{-2}$	$1.29 \times 10^{-2}$	$9.61 \times 10^{-2}$	$1.78 \times 10^{-2}$	$1.09 \times 10^{-1}$	$5.47 \times 10^{-2}$
	25V (SB)	$2.15 \times 10^{-1}$	$1.08 \times 10^{-1}$	$3.47 \times 10^{-2}$	$1.73 \times 10^{-2}$	$1.49 \times 10^{-1}$	$2.36 \times 10^{-2}$	$1.10 \times 10^{-1}$	$5.48 \times 10^{-2}$
	30W (TB)	$1.14 \times 10^{-1}$	$5.71 \times 10^{-2}$	$2.21 \times 10^{-2}$	$1.10 \times 10^{-2}$	$8.01 \times 10^{-2}$	$1.54 \times 10^{-2}$	$9.16 \times 10^{-2}$	$4.58 \times 10^{-2}$
	30V (SB)	$1.98 \times 10^{-1}$	$9.92 \times 10^{-2}$	$2.98 \times 10^{-2}$	$1.49 \times 10^{-2}$	$1.37 \times 10^{-1}$	$2.01 \times 10^{-2}$	$9.16 \times 10^{-2}$	$4.58 \times 10^{-2}$
	35W (TB)	$1.04 \times 10^{-1}$	$5.21 \times 10^{-2}$	$1.91 \times 10^{-2}$	$9.57 \times 10^{-3}$	$7.30 \times 10^{-2}$	$1.32 \times 10^{-2}$	$7.59 \times 10^{-2}$	$3.80 \times 10^{-2}$
	35V (SB)	$1.70 \times 10^{-1}$	$8.50 \times 10^{-2}$	$2.61 \times 10^{-2}$	$1.31 \times 10^{-2}$	$1.17 \times 10^{-1}$	$1.77 \times 10^{-2}$	$7.59 \times 10^{-2}$	$3.80 \times 10^{-2}$
	45W (TB)	$9.11 \times 10^{-2}$	$4.56 \times 10^{-2}$	$1.69 \times 10^{-2}$	$8.44 \times 10^{-3}$	$6.38 \times 10^{-2}$	$1.17 \times 10^{-2}$	$5.67 \times 10^{-2}$	$2.83 \times 10^{-2}$
	55W (TB)	$6.85 \times 10^{-2}$	$3.42 \times 10^{-2}$	$1.37 \times 10^{-2}$	$6.86 \times 10^{-3}$	$4.80 \times 10^{-2}$	$9.57 \times 10^{-3}$	$5.38 \times 10^{-2}$	$2.69 \times 10^{-2}$
NR-X	25	$1.19 \times 10^{-1}$	$7.64 \times 10^{-2}$	$2.24 \times 10^{-2}$	$1.43 \times 10^{-2}$	$7.47 \times 10^{-2}$	$1.41 \times 10^{-2}$	$9.69 \times 10^{-2}$	$6.20 \times 10^{-2}$
	25L	$9.18 \times 10^{-2}$	$5.87 \times 10^{-2}$	$1.85 \times 10^{-2}$	$1.18 \times 10^{-2}$	$5.78 \times 10^{-2}$	$1.17 \times 10^{-2}$	$9.69 \times 10^{-2}$	$6.21 \times 10^{-2}$
	30	$9.95 \times 10^{-2}$	$6.37 \times 10^{-2}$	$1.90 \times 10^{-2}$	$1.21 \times 10^{-2}$	$6.23 \times 10^{-2}$	$1.19 \times 10^{-2}$	$8.55 \times 10^{-2}$	$5.47 \times 10^{-2}$
	30L	$7.65 \times 10^{-2}$	$4.89 \times 10^{-2}$	$1.57 \times 10^{-2}$	$1.00 \times 10^{-2}$	$4.82 \times 10^{-2}$	$9.91 \times 10^{-3}$	$8.55 \times 10^{-2}$	$5.47 \times 10^{-2}$
	35	$9.08 \times 10^{-2}$	$5.81 \times 10^{-2}$	$1.69 \times 10^{-2}$	$1.08 \times 10^{-2}$	$5.67 \times 10^{-2}$	$1.06 \times 10^{-2}$	$7.17 \times 10^{-2}$	$4.59 \times 10^{-2}$
	35L	$6.88 \times 10^{-2}$	$4.40 \times 10^{-2}$	$1.40 \times 10^{-2}$	$8.96 \times 10^{-3}$	$4.32 \times 10^{-2}$	$8.81 \times 10^{-3}$	$7.17 \times 10^{-2}$	$4.59 \times 10^{-2}$
	45	$7.02 \times 10^{-2}$	$4.50 \times 10^{-2}$	$1.35 \times 10^{-2}$	$8.64 \times 10^{-3}$	$4.37 \times 10^{-2}$	$8.39 \times 10^{-3}$	$5.31 \times 10^{-2}$	$3.40 \times 10^{-2}$
	45L	$5.25 \times 10^{-2}$	$3.36 \times 10^{-2}$	$1.11 \times 10^{-2}$	$7.11 \times 10^{-3}$	$3.31 \times 10^{-2}$	$7.05 \times 10^{-3}$	$5.32 \times 10^{-2}$	$3.41 \times 10^{-2}$
	55	$5.92 \times 10^{-2}$	$3.79 \times 10^{-2}$	$1.15 \times 10^{-2}$	$7.36 \times 10^{-3}$	$3.72 \times 10^{-2}$	$7.21 \times 10^{-3}$	$4.66 \times 10^{-2}$	$2.98 \times 10^{-2}$
	55L	$4.66 \times 10^{-2}$	$2.98 \times 10^{-2}$	$9.43 \times 10^{-3}$	$6.02 \times 10^{-3}$	$2.92 \times 10^{-2}$	$5.93 \times 10^{-3}$	$4.65 \times 10^{-2}$	$2.98 \times 10^{-2}$
NR	65	$5.12 \times 10^{-2}$	$3.28 \times 10^{-2}$	$1.00 \times 10^{-2}$	$6.40 \times 10^{-3}$	$3.21 \times 10^{-2}$	$6.31 \times 10^{-3}$	$3.93 \times 10^{-2}$	$2.52 \times 10^{-2}$
	65L	$3.66 \times 10^{-2}$	$2.34 \times 10^{-2}$	$7.73 \times 10^{-3}$	$4.93 \times 10^{-3}$	$2.31 \times 10^{-2}$	$4.89 \times 10^{-3}$	$3.93 \times 10^{-2}$	$2.52 \times 10^{-2}$
	75	$4.21 \times 10^{-2}$	$2.99 \times 10^{-2}$	$8.31 \times 10^{-3}$	$5.90 \times 10^{-3}$	$3.08 \times 10^{-2}$	$6.13 \times 10^{-3}$	$3.16 \times 10^{-2}$	$2.24 \times 10^{-2}$
	75L	$3.14 \times 10^{-2}$	$2.23 \times 10^{-2}$	$6.74 \times 10^{-3}$	$4.78 \times 10^{-3}$	$2.33 \times 10^{-2}$	$5.04 \times 10^{-3}$	$3.16 \times 10^{-2}$	$2.24 \times 10^{-2}$
	85	$3.70 \times 10^{-2}$	$2.62 \times 10^{-2}$	$7.31 \times 10^{-3}$	$5.19 \times 10^{-3}$	$2.71 \times 10^{-2}$	$5.40 \times 10^{-3}$	$2.80 \times 10^{-2}$	$1.99 \times 10^{-2}$
	85L	$2.80 \times 10^{-2}$	$1.99 \times 10^{-2}$	$6.07 \times 10^{-3}$	$4.31 \times 10^{-3}$	$2.08 \times 10^{-2}$	$4.55 \times 10^{-3}$	$2.80 \times 10^{-2}$	$1.99 \times 10^{-2}$
	100	$3.05 \times 10^{-2}$	$2.17 \times 10^{-2}$	$6.20 \times 10^{-3}$	$4.41 \times 10^{-3}$	$2.26 \times 10^{-2}$	$4.63 \times 10^{-3}$	$2.38 \times 10^{-2}$	$1.69 \times 10^{-2}$
	100L	$2.74 \times 10^{-2}$	$1.95 \times 10^{-2}$	$5.46 \times 10^{-3}$	$3.87 \times 10^{-3}$	$2.00 \times 10^{-2}$	$4.00 \times 10^{-3}$	$2.38 \times 10^{-2}$	$1.69 \times 10^{-2}$

$K_{AR1}$  : Equivalent factor in the  $M_A$  radial direction when one LM block is used

$K_{AL1}$  : Equivalent factor in the  $M_A$  reverse-radial direction when one LM block is used

$K_{AR2}$  : Equivalent factor in the  $M_A$  radial direction when two LM blocks are used in close contact with each other

$K_{AL2}$  : Equivalent factor in the  $M_A$  reverse-radial direction when two LM blocks are used in close contact with each other

$K_{B1}$  :  $M_B$  Equivalent factor when one LM block is used

$K_{B2}$  :  $M_B$  Equivalent factor when two LM blocks are used in close contact with each other

$K_{CR}$  : Equivalent factor in the  $M_C$  radial direction

$K_{CL}$  : Equivalent factor in the  $M_C$  reverse-radial direction



Table 4: Equivalent Factors (Models NRS-X, NRS, HRW, and RSX)

Model No.		Equivalent factor							
		K <sub>AR1</sub>	K <sub>AL1</sub>	K <sub>AR2</sub>	K <sub>AL2</sub>	K <sub>B1</sub>	K <sub>B2</sub>	K <sub>CR</sub>	K <sub>CL</sub>
NRS-X	25	$1.15 \times 10^{-3}$	$9.66 \times 10^{-2}$	$2.16 \times 10^{-2}$	$1.81 \times 10^{-2}$	$1.06 \times 10^{-1}$	$1.98 \times 10^{-2}$	$9.51 \times 10^{-2}$	$7.99 \times 10^{-2}$
	25L	$8.85 \times 10^{-2}$	$7.44 \times 10^{-2}$	$1.79 \times 10^{-2}$	$1.50 \times 10^{-2}$	$8.14 \times 10^{-2}$	$1.64 \times 10^{-2}$	$9.51 \times 10^{-2}$	$7.99 \times 10^{-2}$
	30	$9.58 \times 10^{-2}$	$8.05 \times 10^{-2}$	$1.83 \times 10^{-2}$	$1.53 \times 10^{-2}$	$8.81 \times 10^{-2}$	$1.68 \times 10^{-2}$	$8.40 \times 10^{-2}$	$7.05 \times 10^{-2}$
	30L	$7.38 \times 10^{-2}$	$6.20 \times 10^{-2}$	$1.51 \times 10^{-2}$	$1.27 \times 10^{-2}$	$6.79 \times 10^{-2}$	$1.39 \times 10^{-2}$	$8.40 \times 10^{-2}$	$7.05 \times 10^{-2}$
	35	$8.73 \times 10^{-2}$	$7.33 \times 10^{-2}$	$1.62 \times 10^{-2}$	$1.36 \times 10^{-2}$	$8.03 \times 10^{-2}$	$1.49 \times 10^{-2}$	$7.04 \times 10^{-2}$	$5.91 \times 10^{-2}$
	35L	$6.63 \times 10^{-2}$	$5.57 \times 10^{-2}$	$1.35 \times 10^{-2}$	$1.13 \times 10^{-2}$	$6.10 \times 10^{-2}$	$1.24 \times 10^{-2}$	$7.04 \times 10^{-2}$	$5.91 \times 10^{-2}$
	45	$6.78 \times 10^{-2}$	$5.69 \times 10^{-2}$	$1.30 \times 10^{-2}$	$1.09 \times 10^{-2}$	$6.23 \times 10^{-2}$	$1.19 \times 10^{-2}$	$5.22 \times 10^{-2}$	$4.39 \times 10^{-2}$
	45L	$5.07 \times 10^{-2}$	$4.26 \times 10^{-2}$	$1.07 \times 10^{-2}$	$8.99 \times 10^{-3}$	$4.66 \times 10^{-2}$	$9.86 \times 10^{-3}$	$5.22 \times 10^{-2}$	$4.39 \times 10^{-2}$
	55	$5.71 \times 10^{-2}$	$4.79 \times 10^{-2}$	$1.10 \times 10^{-2}$	$9.24 \times 10^{-3}$	$5.25 \times 10^{-2}$	$1.01 \times 10^{-2}$	$4.58 \times 10^{-2}$	$3.84 \times 10^{-2}$
	55L	$4.50 \times 10^{-2}$	$3.78 \times 10^{-2}$	$9.14 \times 10^{-3}$	$7.65 \times 10^{-3}$	$4.14 \times 10^{-2}$	$8.39 \times 10^{-3}$	$4.57 \times 10^{-2}$	$3.84 \times 10^{-2}$
	65	$4.93 \times 10^{-2}$	$4.14 \times 10^{-2}$	$9.70 \times 10^{-3}$	$8.15 \times 10^{-3}$	$4.53 \times 10^{-2}$	$8.88 \times 10^{-3}$	$3.86 \times 10^{-2}$	$3.25 \times 10^{-2}$
65L	$3.54 \times 10^{-2}$	$2.97 \times 10^{-2}$	$7.47 \times 10^{-3}$	$6.30 \times 10^{-3}$	$3.25 \times 10^{-2}$	$6.86 \times 10^{-3}$	$3.86 \times 10^{-2}$	$3.25 \times 10^{-2}$	
NRS	75	$4.05 \times 10^{-2}$		$8.01 \times 10^{-3}$		$4.05 \times 10^{-2}$	$8.01 \times 10^{-3}$		$3.20 \times 10^{-2}$
	75L	$3.03 \times 10^{-2}$		$6.50 \times 10^{-3}$		$3.03 \times 10^{-2}$	$6.50 \times 10^{-3}$		$3.20 \times 10^{-2}$
	85	$3.56 \times 10^{-2}$		$7.05 \times 10^{-3}$		$3.56 \times 10^{-2}$	$7.05 \times 10^{-3}$		$2.83 \times 10^{-2}$
	85L	$2.70 \times 10^{-2}$		$5.87 \times 10^{-3}$		$2.70 \times 10^{-2}$	$5.87 \times 10^{-3}$		$2.83 \times 10^{-2}$
	100	$2.93 \times 10^{-2}$		$5.97 \times 10^{-3}$		$2.93 \times 10^{-2}$	$5.97 \times 10^{-3}$		$2.41 \times 10^{-2}$
	100L	$2.65 \times 10^{-2}$		$5.27 \times 10^{-3}$		$2.65 \times 10^{-2}$	$5.27 \times 10^{-3}$		$2.41 \times 10^{-2}$
HRW	12	$2.72 \times 10^{-1}$	$1.93 \times 10^{-1}$	$5.16 \times 10^{-2}$	$3.65 \times 10^{-2}$	$5.47 \times 10^{-1}$	$1.04 \times 10^{-1}$	$1.40 \times 10^{-1}$	$9.92 \times 10^{-2}$
	14	$2.28 \times 10^{-1}$	$1.61 \times 10^{-1}$	$4.16 \times 10^{-2}$	$2.94 \times 10^{-2}$	$4.54 \times 10^{-1}$	$8.28 \times 10^{-2}$	$1.01 \times 10^{-1}$	$7.18 \times 10^{-2}$
	17	$1.96 \times 10^{-1}$		$3.34 \times 10^{-2}$		$1.96 \times 10^{-1}$	$3.34 \times 10^{-2}$		$6.30 \times 10^{-2}$
	21	$1.65 \times 10^{-1}$		$2.90 \times 10^{-2}$		$1.65 \times 10^{-1}$	$2.90 \times 10^{-2}$		$5.89 \times 10^{-2}$
	27	$1.30 \times 10^{-1}$		$2.34 \times 10^{-2}$		$1.30 \times 10^{-1}$	$2.34 \times 10^{-2}$		$5.11 \times 10^{-2}$
	35	$8.69 \times 10^{-2}$		$1.60 \times 10^{-2}$		$8.69 \times 10^{-2}$	$1.60 \times 10^{-2}$		$3.06 \times 10^{-2}$
	50	$6.52 \times 10^{-2}$		$1.22 \times 10^{-2}$		$6.52 \times 10^{-2}$	$1.22 \times 10^{-2}$		$2.35 \times 10^{-2}$
	60	$5.80 \times 10^{-2}$		$1.08 \times 10^{-2}$		$5.80 \times 10^{-2}$	$1.08 \times 10^{-2}$		$1.77 \times 10^{-2}$

## Selection Criteria

## Calculating the Applied Load

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
RSX	5M	$6.68 \times 10^{-1}$		$9.11 \times 10^{-2}$		$6.80 \times 10^{-1}$	$9.24 \times 10^{-2}$		$3.86 \times 10^{-1}$
	5NM	$5.25 \times 10^{-1}$		$8.01 \times 10^{-2}$		$5.36 \times 10^{-1}$	$8.12 \times 10^{-2}$		$3.86 \times 10^{-1}$
	5WM	$4.58 \times 10^{-1}$		$7.39 \times 10^{-2}$		$4.65 \times 10^{-1}$	$7.51 \times 10^{-2}$		$1.96 \times 10^{-1}$
	5WNM	$3.31 \times 10^{-1}$		$5.98 \times 10^{-2}$		$3.36 \times 10^{-1}$	$6.06 \times 10^{-2}$		$1.96 \times 10^{-1}$
	7SM	$5.90 \times 10^{-1}$		$7.87 \times 10^{-2}$		$6.12 \times 10^{-1}$	$8.15 \times 10^{-2}$		$2.59 \times 10^{-1}$
	7M	$4.72 \times 10^{-1}$		$6.68 \times 10^{-2}$		$4.87 \times 10^{-1}$	$6.88 \times 10^{-2}$		$2.59 \times 10^{-1}$
	7NM	$3.10 \times 10^{-1}$		$5.18 \times 10^{-2}$		$3.20 \times 10^{-1}$	$5.33 \times 10^{-2}$		$2.59 \times 10^{-1}$
	7WSM	$5.23 \times 10^{-1}$		$6.75 \times 10^{-2}$		$5.43 \times 10^{-1}$	$6.95 \times 10^{-2}$		$1.36 \times 10^{-1}$
	7WM	$3.10 \times 10^{-1}$		$5.34 \times 10^{-2}$		$3.20 \times 10^{-1}$	$5.50 \times 10^{-2}$		$1.36 \times 10^{-1}$
	7WNM	$2.21 \times 10^{-1}$		$4.18 \times 10^{-2}$		$2.27 \times 10^{-1}$	$4.32 \times 10^{-2}$		$1.36 \times 10^{-1}$
	9SM	$5.37 \times 10^{-1}$		$6.77 \times 10^{-2}$		$5.57 \times 10^{-1}$	$7.00 \times 10^{-2}$		$2.17 \times 10^{-1}$
	9M	$3.10 \times 10^{-1}$		$5.28 \times 10^{-2}$		$3.19 \times 10^{-1}$	$5.44 \times 10^{-2}$		$2.17 \times 10^{-1}$
	9NM	$2.17 \times 10^{-1}$		$4.13 \times 10^{-2}$		$2.24 \times 10^{-1}$	$4.27 \times 10^{-2}$		$2.17 \times 10^{-1}$
	9WSM	$4.16 \times 10^{-1}$		$5.80 \times 10^{-2}$		$4.30 \times 10^{-1}$	$5.98 \times 10^{-2}$		$1.06 \times 10^{-1}$
	9WM	$2.31 \times 10^{-1}$		$4.31 \times 10^{-2}$		$2.38 \times 10^{-1}$	$4.43 \times 10^{-2}$		$1.06 \times 10^{-1}$
	9WNM	$1.75 \times 10^{-1}$		$3.38 \times 10^{-2}$		$1.81 \times 10^{-1}$	$3.48 \times 10^{-2}$		$1.06 \times 10^{-1}$
	12SM	$5.04 \times 10^{-1}$		$5.52 \times 10^{-2}$		$5.04 \times 10^{-1}$	$5.52 \times 10^{-2}$		$1.52 \times 10^{-1}$
	12M	$2.96 \times 10^{-1}$		$4.55 \times 10^{-2}$		$2.96 \times 10^{-1}$	$4.55 \times 10^{-2}$		$1.52 \times 10^{-1}$
	12NM	$1.96 \times 10^{-1}$		$3.50 \times 10^{-2}$		$1.96 \times 10^{-1}$	$3.50 \times 10^{-2}$		$1.52 \times 10^{-1}$
	12WSM	$3.32 \times 10^{-1}$		$5.07 \times 10^{-2}$		$3.32 \times 10^{-1}$	$5.07 \times 10^{-2}$		$7.95 \times 10^{-2}$
	12WM	$2.10 \times 10^{-1}$		$3.69 \times 10^{-2}$		$2.10 \times 10^{-1}$	$3.69 \times 10^{-2}$		$7.95 \times 10^{-2}$
	12WNM	$1.46 \times 10^{-1}$		$2.85 \times 10^{-2}$		$1.46 \times 10^{-1}$	$2.85 \times 10^{-2}$		$7.95 \times 10^{-2}$
	15SM	$3.36 \times 10^{-1}$		$4.58 \times 10^{-2}$		$3.36 \times 10^{-1}$	$4.58 \times 10^{-2}$		$1.41 \times 10^{-1}$
	15M	$2.34 \times 10^{-1}$		$3.65 \times 10^{-2}$		$2.34 \times 10^{-1}$	$3.65 \times 10^{-2}$		$1.41 \times 10^{-1}$
	15NM	$1.45 \times 10^{-1}$		$2.75 \times 10^{-2}$		$1.45 \times 10^{-1}$	$2.75 \times 10^{-2}$		$1.41 \times 10^{-1}$
	15WSM	$2.34 \times 10^{-1}$		$3.81 \times 10^{-2}$		$2.34 \times 10^{-1}$	$3.81 \times 10^{-2}$		$4.82 \times 10^{-2}$
	15WM	$1.66 \times 10^{-1}$		$2.97 \times 10^{-2}$		$1.66 \times 10^{-1}$	$2.97 \times 10^{-2}$		$4.82 \times 10^{-2}$
	15WNM	$1.15 \times 10^{-1}$		$2.28 \times 10^{-2}$		$1.15 \times 10^{-1}$	$2.28 \times 10^{-2}$		$4.82 \times 10^{-2}$
	9M1	$3.10 \times 10^{-1}$		$5.28 \times 10^{-2}$		$3.19 \times 10^{-1}$	$5.44 \times 10^{-2}$		$2.17 \times 10^{-1}$
	9M1N	$2.17 \times 10^{-1}$		$4.13 \times 10^{-2}$		$2.24 \times 10^{-1}$	$4.27 \times 10^{-2}$		$2.17 \times 10^{-1}$
9M1W	$2.31 \times 10^{-1}$		$4.31 \times 10^{-2}$		$2.38 \times 10^{-1}$	$4.43 \times 10^{-2}$		$1.06 \times 10^{-1}$	
9M1WN	$1.75 \times 10^{-1}$		$3.38 \times 10^{-2}$		$1.81 \times 10^{-1}$	$3.48 \times 10^{-2}$		$1.06 \times 10^{-1}$	
12M1	$2.96 \times 10^{-1}$		$4.55 \times 10^{-2}$		$2.96 \times 10^{-1}$	$4.55 \times 10^{-2}$		$1.52 \times 10^{-1}$	
12M1N	$1.96 \times 10^{-1}$		$3.50 \times 10^{-2}$		$1.96 \times 10^{-1}$	$3.50 \times 10^{-2}$		$1.52 \times 10^{-1}$	
12M1W	$2.10 \times 10^{-1}$		$3.69 \times 10^{-2}$		$2.10 \times 10^{-1}$	$3.69 \times 10^{-2}$		$7.95 \times 10^{-2}$	
12M1WN	$1.46 \times 10^{-1}$		$2.85 \times 10^{-2}$		$1.46 \times 10^{-1}$	$2.85 \times 10^{-2}$		$7.95 \times 10^{-2}$	
15M1	$2.34 \times 10^{-1}$		$3.65 \times 10^{-2}$		$2.34 \times 10^{-1}$	$3.65 \times 10^{-2}$		$1.41 \times 10^{-1}$	
15M1N	$1.45 \times 10^{-1}$		$2.75 \times 10^{-2}$		$1.45 \times 10^{-1}$	$2.75 \times 10^{-2}$		$1.41 \times 10^{-1}$	
15M1W	$1.66 \times 10^{-1}$		$2.97 \times 10^{-2}$		$1.66 \times 10^{-1}$	$2.97 \times 10^{-2}$		$4.82 \times 10^{-2}$	
15M1WN	$1.15 \times 10^{-1}$		$2.28 \times 10^{-2}$		$1.15 \times 10^{-1}$	$2.28 \times 10^{-2}$		$4.82 \times 10^{-2}$	

$K_{AR1}$  : Equivalent factor in the  $M_A$  radial direction when one LM block is used

$K_{AL1}$  : Equivalent factor in the  $M_A$  reverse-radial direction when one LM block is used

$K_{AR2}$  : Equivalent factor in the  $M_A$  radial direction when two LM blocks are used in close contact with each other

$K_{AL2}$  : Equivalent factor in the  $M_A$  reverse-radial direction when two LM blocks are used in close contact with each other

$K_{B1}$  :  $M_B$  Equivalent factor when one LM block is used

$K_{B2}$  :  $M_B$  Equivalent factor when two LM blocks are used in close contact with each other

$K_{CR}$  : Equivalent factor in the  $M_C$  radial direction

$K_{CL}$  : Equivalent factor in the  $M_C$  reverse-radial direction

Table 5: Equivalent Factors (Models RSR and HR)

Model No.	Equivalent factor								
	$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$	
RSR	2N	$6.81 \times 10^{-1}$		$1.28 \times 10^{-1}$		$6.81 \times 10^{-1}$	$1.28 \times 10^{-1}$	$8.69 \times 10^{-1}$	
	2WN	$5.10 \times 10^{-1}$		$9.32 \times 10^{-2}$		$5.10 \times 10^{-1}$	$9.32 \times 10^{-2}$	$4.54 \times 10^{-1}$	
	3M	$9.20 \times 10^{-1}$		$1.27 \times 10^{-1}$		$9.20 \times 10^{-1}$	$1.27 \times 10^{-1}$	$6.06 \times 10^{-1}$	
	3N	$6.06 \times 10^{-1}$		$1.01 \times 10^{-1}$		$6.06 \times 10^{-1}$	$1.01 \times 10^{-1}$	$6.06 \times 10^{-1}$	
	3W	$7.03 \times 10^{-1}$		$1.06 \times 10^{-1}$		$7.03 \times 10^{-1}$	$1.06 \times 10^{-1}$	$3.17 \times 10^{-1}$	
	3WN	$4.76 \times 10^{-1}$		$8.27 \times 10^{-2}$		$4.76 \times 10^{-1}$	$8.27 \times 10^{-2}$	$3.17 \times 10^{-1}$	
	9M1K	$3.06 \times 10^{-1}$		$5.19 \times 10^{-2}$		$3.06 \times 10^{-1}$	$5.19 \times 10^{-2}$	$2.15 \times 10^{-1}$	
	9M1N	$2.15 \times 10^{-1}$		$4.08 \times 10^{-2}$		$2.15 \times 10^{-1}$	$4.08 \times 10^{-2}$	$2.15 \times 10^{-1}$	
	9M1WV	$2.44 \times 10^{-1}$		$4.22 \times 10^{-2}$		$2.44 \times 10^{-1}$	$4.22 \times 10^{-2}$	$1.09 \times 10^{-1}$	
	9M1WN	$1.73 \times 10^{-1}$		$3.33 \times 10^{-2}$		$1.73 \times 10^{-1}$	$3.33 \times 10^{-2}$	$1.09 \times 10^{-1}$	
	12M1V	$3.52 \times 10^{-1}$	$2.46 \times 10^{-1}$	$5.37 \times 10^{-2}$	$3.76 \times 10^{-2}$	$2.81 \times 10^{-1}$	$4.21 \times 10^{-2}$	$2.09 \times 10^{-1}$	$1.46 \times 10^{-1}$
	12M1N	$2.30 \times 10^{-1}$	$1.61 \times 10^{-1}$	$4.08 \times 10^{-2}$	$2.85 \times 10^{-2}$	$1.85 \times 10^{-1}$	$3.25 \times 10^{-2}$	$2.09 \times 10^{-1}$	$1.46 \times 10^{-1}$
	12M1WV	$2.47 \times 10^{-1}$	$1.73 \times 10^{-1}$	$4.38 \times 10^{-2}$	$3.07 \times 10^{-2}$	$1.99 \times 10^{-1}$	$3.49 \times 10^{-2}$	$1.02 \times 10^{-1}$	$7.15 \times 10^{-2}$
	12M1WN	$1.71 \times 10^{-1}$	$1.20 \times 10^{-1}$	$3.36 \times 10^{-2}$	$2.35 \times 10^{-2}$	$1.38 \times 10^{-1}$	$2.70 \times 10^{-2}$	$1.02 \times 10^{-1}$	$7.15 \times 10^{-2}$
	14WV	$2.10 \times 10^{-1}$	$1.47 \times 10^{-1}$	$3.89 \times 10^{-2}$	$2.73 \times 10^{-2}$	$1.69 \times 10^{-1}$	$3.10 \times 10^{-2}$	$8.22 \times 10^{-2}$	$5.75 \times 10^{-2}$
	15M1V	$2.77 \times 10^{-1}$	$1.94 \times 10^{-1}$	$4.38 \times 10^{-2}$	$3.07 \times 10^{-2}$	$2.21 \times 10^{-1}$	$3.45 \times 10^{-2}$	$1.69 \times 10^{-1}$	$1.18 \times 10^{-1}$
	15M1N	$1.70 \times 10^{-1}$	$1.19 \times 10^{-1}$	$3.24 \times 10^{-2}$	$2.27 \times 10^{-2}$	$1.37 \times 10^{-1}$	$2.59 \times 10^{-2}$	$1.69 \times 10^{-1}$	$1.18 \times 10^{-1}$
	15M1WV	$1.95 \times 10^{-1}$	$1.36 \times 10^{-1}$	$3.52 \times 10^{-2}$	$2.46 \times 10^{-2}$	$1.56 \times 10^{-1}$	$2.80 \times 10^{-2}$	$5.83 \times 10^{-2}$	$4.08 \times 10^{-2}$
	15M1WN	$1.34 \times 10^{-1}$	$9.41 \times 10^{-2}$	$2.68 \times 10^{-2}$	$1.88 \times 10^{-2}$	$1.09 \times 10^{-1}$	$2.16 \times 10^{-2}$	$5.82 \times 10^{-2}$	$4.08 \times 10^{-2}$
	20M1V	$1.68 \times 10^{-1}$	$1.18 \times 10^{-1}$	$2.92 \times 10^{-2}$	$2.04 \times 10^{-2}$	$1.35 \times 10^{-1}$	$2.32 \times 10^{-2}$	$1.30 \times 10^{-1}$	$9.13 \times 10^{-2}$
20M1N	$1.20 \times 10^{-1}$	$8.39 \times 10^{-2}$	$2.30 \times 10^{-2}$	$1.61 \times 10^{-2}$	$9.68 \times 10^{-2}$	$1.84 \times 10^{-2}$	$1.30 \times 10^{-1}$	$9.13 \times 10^{-2}$	
HR	918	$2.65 \times 10^{-1}$		$3.58 \times 10^{-2}$		$2.65 \times 10^{-1}$	$3.58 \times 10^{-2}$	—	—
	1123	$2.08 \times 10^{-1}$		$3.17 \times 10^{-2}$		$2.08 \times 10^{-1}$	$3.17 \times 10^{-2}$	—	—
	1530	$1.56 \times 10^{-1}$		$2.39 \times 10^{-2}$		$1.56 \times 10^{-1}$	$2.39 \times 10^{-2}$	—	—
	2042	$1.11 \times 10^{-1}$		$1.80 \times 10^{-2}$		$1.11 \times 10^{-1}$	$1.80 \times 10^{-2}$	—	—
	2042T	$8.64 \times 10^{-2}$		$1.53 \times 10^{-2}$		$8.64 \times 10^{-2}$	$1.53 \times 10^{-2}$	—	—
	2555	$7.79 \times 10^{-2}$		$1.38 \times 10^{-2}$		$7.79 \times 10^{-2}$	$1.38 \times 10^{-2}$	—	—
	2555T	$6.13 \times 10^{-2}$		$1.17 \times 10^{-2}$		$6.13 \times 10^{-2}$	$1.17 \times 10^{-2}$	—	—
	3065	$6.92 \times 10^{-2}$		$1.15 \times 10^{-2}$		$6.92 \times 10^{-2}$	$1.15 \times 10^{-2}$	—	—
	3065T	$5.45 \times 10^{-2}$		$9.92 \times 10^{-3}$		$5.45 \times 10^{-2}$	$9.92 \times 10^{-3}$	—	—
	3575	$6.23 \times 10^{-2}$		$1.08 \times 10^{-2}$		$6.23 \times 10^{-2}$	$1.08 \times 10^{-2}$	—	—
	3575T	$4.90 \times 10^{-2}$		$9.42 \times 10^{-3}$		$4.90 \times 10^{-2}$	$9.42 \times 10^{-3}$	—	—
	4085	$5.19 \times 10^{-2}$		$9.53 \times 10^{-3}$		$5.19 \times 10^{-2}$	$9.53 \times 10^{-3}$	—	—
	4085T	$4.09 \times 10^{-2}$		$7.97 \times 10^{-3}$		$4.09 \times 10^{-2}$	$7.97 \times 10^{-3}$	—	—
	50105	$4.15 \times 10^{-2}$		$7.40 \times 10^{-3}$		$4.15 \times 10^{-2}$	$7.40 \times 10^{-3}$	—	—
	50105T	$3.27 \times 10^{-2}$		$6.26 \times 10^{-3}$		$3.27 \times 10^{-2}$	$6.26 \times 10^{-3}$	—	—
	60125	$2.88 \times 10^{-2}$		$5.18 \times 10^{-3}$		$2.88 \times 10^{-2}$	$5.18 \times 10^{-3}$	—	—

$K_{AR1}$  : Equivalent factor in the  $M_x$  radial direction when one LM block is used

$K_{AL1}$  : Equivalent factor in the  $M_x$  reverse-radial direction when one LM block is used

$K_{AR2}$  : Equivalent factor in the  $M_x$  radial direction when two LM blocks are used in close contact with each other

$K_{AL2}$  : Equivalent factor in the  $M_x$  reverse-radial direction when two LM blocks are used in close contact with each other

$K_{B1}$  :  $M_s$  Equivalent factor when one LM block is used

$K_{B2}$  :  $M_s$  Equivalent factor when two LM blocks are used in close contact with each other

$K_{CR}$  : Equivalent factor in the  $M_c$  radial direction

$K_{CL}$  : Equivalent factor in the  $M_c$  reverse-radial direction

## Selection Criteria

## Calculating the Applied Load

Table 6: Equivalent Factors (Models GSR, CSR, MX, JR, NSR, SRG, SRN, SRW, and HRX)

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
GSR	15T	$1.61 \times 10^{-1}$	$1.44 \times 10^{-1}$	$2.88 \times 10^{-2}$	$2.59 \times 10^{-2}$	$1.68 \times 10^{-1}$	$3.01 \times 10^{-2}$	—	—
	15V	$2.21 \times 10^{-1}$	$1.99 \times 10^{-1}$	$3.54 \times 10^{-2}$	$3.18 \times 10^{-2}$	$2.30 \times 10^{-1}$	$3.68 \times 10^{-2}$	—	—
	20T	$1.28 \times 10^{-1}$	$1.16 \times 10^{-1}$	$2.34 \times 10^{-2}$	$2.10 \times 10^{-2}$	$1.34 \times 10^{-1}$	$2.44 \times 10^{-2}$	—	—
	20V	$1.77 \times 10^{-1}$	$1.59 \times 10^{-1}$	$2.87 \times 10^{-2}$	$2.58 \times 10^{-2}$	$1.84 \times 10^{-1}$	$2.99 \times 10^{-2}$	—	—
	25T	$1.07 \times 10^{-1}$	$9.63 \times 10^{-2}$	$1.97 \times 10^{-2}$	$1.77 \times 10^{-2}$	$1.12 \times 10^{-1}$	$2.06 \times 10^{-2}$	—	—
	25V	$1.47 \times 10^{-1}$	$1.33 \times 10^{-1}$	$2.42 \times 10^{-2}$	$2.18 \times 10^{-2}$	$1.53 \times 10^{-1}$	$2.52 \times 10^{-2}$	—	—
	30T	$9.17 \times 10^{-2}$	$8.26 \times 10^{-2}$	$1.68 \times 10^{-2}$	$1.51 \times 10^{-2}$	$9.59 \times 10^{-2}$	$1.76 \times 10^{-2}$	—	—
	35T	$8.03 \times 10^{-2}$	$7.22 \times 10^{-2}$	$1.48 \times 10^{-2}$	$1.33 \times 10^{-2}$	$8.39 \times 10^{-2}$	$1.55 \times 10^{-2}$	—	—
CSR	15	$1.66 \times 10^{-1}$		—		$1.66 \times 10^{-1}$	—	—	—
	20S	$1.26 \times 10^{-1}$		—		$1.26 \times 10^{-1}$	—	—	—
	20	$9.88 \times 10^{-2}$		—		$9.88 \times 10^{-2}$	—	—	—
	25S	$1.12 \times 10^{-1}$		—		$1.12 \times 10^{-1}$	—	—	—
	25	$8.23 \times 10^{-2}$		—		$8.23 \times 10^{-2}$	—	—	—
	30S	$8.97 \times 10^{-2}$		—		$8.97 \times 10^{-2}$	—	—	—
	30	$7.05 \times 10^{-2}$		—		$7.05 \times 10^{-2}$	—	—	—
	35	$6.17 \times 10^{-2}$		—		$6.17 \times 10^{-2}$	—	—	—
MX	5	$4.27 \times 10^{-1}$		$7.01 \times 10^{-2}$		$4.27 \times 10^{-1}$	$7.01 \times 10^{-2}$	—	—
	7W	$2.18 \times 10^{-1}$		$4.13 \times 10^{-2}$		$2.18 \times 10^{-1}$	$4.13 \times 10^{-2}$	—	—
JR	25	$1.12 \times 10^{-1}$		$2.02 \times 10^{-2}$		$1.12 \times 10^{-1}$	$2.02 \times 10^{-2}$	$9.96 \times 10^{-2}$	—
	35	$7.85 \times 10^{-2}$		$1.56 \times 10^{-2}$		$7.85 \times 10^{-2}$	$1.56 \times 10^{-2}$	$6.69 \times 10^{-2}$	—
	45	$6.73 \times 10^{-2}$		$1.21 \times 10^{-2}$		$6.73 \times 10^{-2}$	$1.21 \times 10^{-2}$	$5.20 \times 10^{-2}$	—
	55	$5.61 \times 10^{-2}$		$1.03 \times 10^{-2}$		$5.61 \times 10^{-2}$	$1.03 \times 10^{-2}$	$4.26 \times 10^{-2}$	—
NSR	20TBC	$2.29 \times 10^{-1}$		$2.68 \times 10^{-2}$		$2.29 \times 10^{-1}$	$2.68 \times 10^{-2}$	—	—
	25TBC	$2.01 \times 10^{-1}$		$2.27 \times 10^{-2}$		$2.01 \times 10^{-1}$	$2.27 \times 10^{-2}$	—	—
	30TBC	$1.85 \times 10^{-1}$		$1.93 \times 10^{-2}$		$1.85 \times 10^{-1}$	$1.93 \times 10^{-2}$	—	—
	40TBC	$1.39 \times 10^{-1}$		$1.60 \times 10^{-2}$		$1.39 \times 10^{-1}$	$1.60 \times 10^{-2}$	—	—
	50TBC	$1.24 \times 10^{-1}$		$1.42 \times 10^{-2}$		$1.24 \times 10^{-1}$	$1.42 \times 10^{-2}$	—	—
	70TBC	$9.99 \times 10^{-2}$		$1.15 \times 10^{-2}$		$9.99 \times 10^{-2}$	$1.15 \times 10^{-2}$	—	—

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
SRG	15X	$1.23 \times 10^{-1}$		$2.07 \times 10^{-2}$		$1.23 \times 10^{-1}$	$2.07 \times 10^{-2}$		$1.04 \times 10^{-1}$
	15XG	$1.25 \times 10^{-1}$		$2.08 \times 10^{-2}$		$1.25 \times 10^{-1}$	$2.08 \times 10^{-2}$		$1.04 \times 10^{-1}$
	20X	$9.60 \times 10^{-2}$		$1.71 \times 10^{-2}$		$9.60 \times 10^{-2}$	$1.71 \times 10^{-2}$		$8.00 \times 10^{-2}$
	20XG	$9.67 \times 10^{-2}$		$1.68 \times 10^{-2}$		$9.67 \times 10^{-2}$	$1.68 \times 10^{-2}$		$8.00 \times 10^{-2}$
	20XL	$7.21 \times 10^{-2}$		$1.42 \times 10^{-2}$		$7.21 \times 10^{-2}$	$1.42 \times 10^{-2}$		$8.00 \times 10^{-2}$
	20XGL	$7.38 \times 10^{-2}$		$1.39 \times 10^{-2}$		$7.38 \times 10^{-2}$	$1.39 \times 10^{-2}$		$8.00 \times 10^{-2}$
	25X	$8.96 \times 10^{-2}$		$1.55 \times 10^{-2}$		$8.96 \times 10^{-2}$	$1.55 \times 10^{-2}$		$7.23 \times 10^{-2}$
	25XG	$8.52 \times 10^{-2}$		$1.51 \times 10^{-2}$		$8.52 \times 10^{-2}$	$1.51 \times 10^{-2}$		$7.23 \times 10^{-2}$
	25XL	$6.99 \times 10^{-2}$		$1.31 \times 10^{-2}$		$6.99 \times 10^{-2}$	$1.31 \times 10^{-2}$		$7.23 \times 10^{-2}$
	25XGL	$6.69 \times 10^{-2}$		$1.27 \times 10^{-2}$		$6.69 \times 10^{-2}$	$1.27 \times 10^{-2}$		$7.23 \times 10^{-2}$
	30X	$8.06 \times 10^{-2}$		$1.33 \times 10^{-2}$		$8.06 \times 10^{-2}$	$1.33 \times 10^{-2}$		$5.61 \times 10^{-2}$
	30XG	$7.90 \times 10^{-2}$		$1.34 \times 10^{-2}$		$7.90 \times 10^{-2}$	$1.34 \times 10^{-2}$		$5.96 \times 10^{-2}$
	30XL	$6.12 \times 10^{-2}$		$1.11 \times 10^{-2}$		$6.12 \times 10^{-2}$	$1.11 \times 10^{-2}$		$5.61 \times 10^{-2}$
	30XGL	$6.15 \times 10^{-2}$		$1.11 \times 10^{-2}$		$6.15 \times 10^{-2}$	$1.11 \times 10^{-2}$		$5.96 \times 10^{-2}$
	35	$7.14 \times 10^{-2}$		$1.18 \times 10^{-2}$		$7.14 \times 10^{-2}$	$1.18 \times 10^{-2}$		$4.98 \times 10^{-2}$
	35G	$7.37 \times 10^{-2}$		$1.17 \times 10^{-2}$		$7.37 \times 10^{-2}$	$1.17 \times 10^{-2}$		$4.86 \times 10^{-2}$
	35L	$5.26 \times 10^{-2}$		$9.67 \times 10^{-3}$		$5.26 \times 10^{-2}$	$9.67 \times 10^{-3}$		$4.98 \times 10^{-2}$
	35GL	$5.37 \times 10^{-2}$		$9.67 \times 10^{-3}$		$5.37 \times 10^{-2}$	$9.67 \times 10^{-3}$		$4.86 \times 10^{-2}$
	35SL	$4.40 \times 10^{-2}$		$8.34 \times 10^{-3}$		$4.40 \times 10^{-2}$	$8.34 \times 10^{-3}$		$4.98 \times 10^{-2}$
	35GSL	$4.43 \times 10^{-2}$		$8.35 \times 10^{-3}$		$4.43 \times 10^{-2}$	$8.35 \times 10^{-3}$		$4.86 \times 10^{-2}$
	45	$5.49 \times 10^{-2}$		$9.58 \times 10^{-3}$		$5.49 \times 10^{-2}$	$9.58 \times 10^{-3}$		$3.85 \times 10^{-2}$
	45G	$5.53 \times 10^{-2}$		$9.60 \times 10^{-3}$		$5.53 \times 10^{-2}$	$9.60 \times 10^{-3}$		$3.68 \times 10^{-2}$
	45L	$4.18 \times 10^{-2}$		$7.93 \times 10^{-3}$		$4.18 \times 10^{-2}$	$7.93 \times 10^{-3}$		$3.85 \times 10^{-2}$
	45GL	$4.19 \times 10^{-2}$		$7.94 \times 10^{-3}$		$4.19 \times 10^{-2}$	$7.94 \times 10^{-3}$		$3.68 \times 10^{-2}$
	45SL	$3.28 \times 10^{-2}$		$6.56 \times 10^{-3}$		$3.28 \times 10^{-2}$	$6.56 \times 10^{-3}$		$3.85 \times 10^{-2}$
	45GSL	$3.30 \times 10^{-2}$		$6.57 \times 10^{-3}$		$3.30 \times 10^{-2}$	$6.57 \times 10^{-3}$		$3.68 \times 10^{-2}$
	55	$4.56 \times 10^{-2}$		$8.04 \times 10^{-3}$		$4.56 \times 10^{-2}$	$8.04 \times 10^{-3}$		$3.25 \times 10^{-2}$
	55G	$4.61 \times 10^{-2}$		$8.05 \times 10^{-3}$		$4.61 \times 10^{-2}$	$8.05 \times 10^{-3}$		$3.14 \times 10^{-2}$
	55L	$3.37 \times 10^{-2}$		$6.42 \times 10^{-3}$		$3.37 \times 10^{-2}$	$6.42 \times 10^{-3}$		$3.25 \times 10^{-2}$
	55GL	$3.40 \times 10^{-2}$		$6.42 \times 10^{-3}$		$3.40 \times 10^{-2}$	$6.42 \times 10^{-3}$		$3.14 \times 10^{-2}$
	55SL	$2.56 \times 10^{-2}$		$5.22 \times 10^{-3}$		$2.56 \times 10^{-2}$	$5.22 \times 10^{-3}$		$3.25 \times 10^{-2}$
	55GSL	$2.59 \times 10^{-2}$		$5.22 \times 10^{-3}$		$2.59 \times 10^{-2}$	$5.22 \times 10^{-3}$		$3.14 \times 10^{-2}$
	65	$3.54 \times 10^{-2}$		$6.06 \times 10^{-3}$		$3.54 \times 10^{-2}$	$6.06 \times 10^{-3}$		$2.70 \times 10^{-2}$
	65G	$3.44 \times 10^{-2}$		$6.10 \times 10^{-3}$		$3.44 \times 10^{-2}$	$6.10 \times 10^{-3}$		$2.63 \times 10^{-2}$
	65L	$2.63 \times 10^{-2}$		$4.97 \times 10^{-3}$		$2.63 \times 10^{-2}$	$4.97 \times 10^{-3}$		$2.70 \times 10^{-2}$
	65GL	$2.65 \times 10^{-2}$		$4.98 \times 10^{-3}$		$2.65 \times 10^{-2}$	$4.98 \times 10^{-3}$		$2.63 \times 10^{-2}$
	65SL	$1.97 \times 10^{-2}$		$4.01 \times 10^{-3}$		$1.97 \times 10^{-2}$	$4.01 \times 10^{-3}$		$2.70 \times 10^{-2}$
	65GSL	$1.99 \times 10^{-2}$		$4.10 \times 10^{-3}$		$1.99 \times 10^{-2}$	$4.10 \times 10^{-3}$		$2.63 \times 10^{-2}$
	85LC	$2.19 \times 10^{-2}$		$4.15 \times 10^{-3}$		$2.19 \times 10^{-2}$	$4.15 \times 10^{-3}$		$1.91 \times 10^{-2}$
	100LC	$1.95 \times 10^{-2}$		$3.67 \times 10^{-3}$		$1.95 \times 10^{-2}$	$3.67 \times 10^{-3}$		$1.62 \times 10^{-2}$
SRN	35	$7.14 \times 10^{-2}$		$1.18 \times 10^{-2}$		$7.14 \times 10^{-2}$	$1.18 \times 10^{-2}$		$4.98 \times 10^{-2}$
	35G	$7.37 \times 10^{-2}$		$1.17 \times 10^{-2}$		$7.37 \times 10^{-2}$	$1.17 \times 10^{-2}$		$4.86 \times 10^{-2}$

## Selection Criteria

## Calculating the Applied Load

Model No.		Equivalent factor							
		$K_{AR1}$	$K_{AL1}$	$K_{AR2}$	$K_{AL2}$	$K_{B1}$	$K_{B2}$	$K_{CR}$	$K_{CL}$
SRN	35L	$5.26 \times 10^{-2}$		$9.67 \times 10^{-3}$		$5.26 \times 10^{-2}$	$9.67 \times 10^{-3}$		$4.98 \times 10^{-2}$
	35GL	$5.37 \times 10^{-2}$		$9.67 \times 10^{-3}$		$5.37 \times 10^{-2}$	$9.67 \times 10^{-3}$		$4.86 \times 10^{-2}$
	35SL	$4.40 \times 10^{-2}$		$8.34 \times 10^{-3}$		$4.40 \times 10^{-2}$	$8.34 \times 10^{-3}$		$4.98 \times 10^{-2}$
	35GSL	$4.43 \times 10^{-2}$		$8.35 \times 10^{-3}$		$4.43 \times 10^{-2}$	$8.35 \times 10^{-3}$		$4.86 \times 10^{-2}$
	45	$5.49 \times 10^{-2}$		$9.58 \times 10^{-3}$		$5.49 \times 10^{-2}$	$9.58 \times 10^{-3}$		$3.85 \times 10^{-2}$
	45G	$5.53 \times 10^{-2}$		$9.60 \times 10^{-3}$		$5.53 \times 10^{-2}$	$9.60 \times 10^{-3}$		$3.68 \times 10^{-2}$
	45L	$4.18 \times 10^{-2}$		$7.93 \times 10^{-3}$		$4.18 \times 10^{-2}$	$7.93 \times 10^{-3}$		$3.85 \times 10^{-2}$
	45GL	$4.19 \times 10^{-2}$		$7.94 \times 10^{-3}$		$4.19 \times 10^{-2}$	$7.94 \times 10^{-3}$		$3.68 \times 10^{-2}$
	45SL	$3.28 \times 10^{-2}$		$6.56 \times 10^{-3}$		$3.28 \times 10^{-2}$	$6.56 \times 10^{-3}$		$3.85 \times 10^{-2}$
	45GSL	$3.30 \times 10^{-2}$		$6.57 \times 10^{-3}$		$3.30 \times 10^{-2}$	$6.57 \times 10^{-3}$		$3.68 \times 10^{-2}$
	55	$4.56 \times 10^{-2}$		$8.04 \times 10^{-3}$		$4.56 \times 10^{-2}$	$8.04 \times 10^{-3}$		$3.25 \times 10^{-2}$
	55G	$4.61 \times 10^{-2}$		$8.05 \times 10^{-3}$		$4.61 \times 10^{-2}$	$8.05 \times 10^{-3}$		$3.14 \times 10^{-2}$
	55L	$3.37 \times 10^{-2}$		$6.42 \times 10^{-3}$		$3.37 \times 10^{-2}$	$6.42 \times 10^{-3}$		$3.25 \times 10^{-2}$
	55GL	$3.40 \times 10^{-2}$		$6.42 \times 10^{-3}$		$3.40 \times 10^{-2}$	$6.42 \times 10^{-3}$		$3.14 \times 10^{-2}$
	55SL	$2.56 \times 10^{-2}$		$5.22 \times 10^{-3}$		$2.56 \times 10^{-2}$	$5.22 \times 10^{-3}$		$3.25 \times 10^{-2}$
	55GSL	$2.59 \times 10^{-2}$		$5.22 \times 10^{-3}$		$2.59 \times 10^{-2}$	$5.22 \times 10^{-3}$		$3.14 \times 10^{-2}$
	65	$3.54 \times 10^{-2}$		$6.06 \times 10^{-3}$		$3.54 \times 10^{-2}$	$6.06 \times 10^{-3}$		$2.70 \times 10^{-2}$
	65G	$3.44 \times 10^{-2}$		$6.10 \times 10^{-3}$		$3.44 \times 10^{-2}$	$6.10 \times 10^{-3}$		$2.63 \times 10^{-2}$
	65L	$2.63 \times 10^{-2}$		$4.97 \times 10^{-3}$		$2.63 \times 10^{-2}$	$4.97 \times 10^{-3}$		$2.70 \times 10^{-2}$
	65GL	$2.65 \times 10^{-2}$		$4.98 \times 10^{-3}$		$2.65 \times 10^{-2}$	$4.98 \times 10^{-3}$		$2.63 \times 10^{-2}$
65SL	$1.97 \times 10^{-2}$		$4.01 \times 10^{-3}$		$1.97 \times 10^{-2}$	$4.01 \times 10^{-3}$		$2.70 \times 10^{-2}$	
65GSL	$1.99 \times 10^{-2}$		$4.10 \times 10^{-3}$		$1.99 \times 10^{-2}$	$4.10 \times 10^{-3}$		$2.63 \times 10^{-2}$	
SRW	70	$4.18 \times 10^{-2}$		$7.93 \times 10^{-3}$		$4.18 \times 10^{-2}$	$7.93 \times 10^{-3}$		$2.52 \times 10^{-2}$
	85	$3.37 \times 10^{-2}$		$6.42 \times 10^{-3}$		$3.37 \times 10^{-2}$	$6.42 \times 10^{-3}$		$2.09 \times 10^{-2}$
	100	$2.63 \times 10^{-2}$		$4.97 \times 10^{-3}$		$2.63 \times 10^{-2}$	$4.97 \times 10^{-3}$		$1.77 \times 10^{-2}$
	130	$2.19 \times 10^{-2}$		$4.15 \times 10^{-3}$		$2.19 \times 10^{-2}$	$4.15 \times 10^{-3}$		$1.33 \times 10^{-2}$
	150	$1.95 \times 10^{-2}$		$3.67 \times 10^{-3}$		$1.95 \times 10^{-2}$	$3.67 \times 10^{-3}$		$1.15 \times 10^{-2}$
HRX	25	$7.91 \times 10^{-2}$		$1.51 \times 10^{-2}$		$7.91 \times 10^{-2}$	$1.51 \times 10^{-2}$	$1.29 \times 10^{-1}$	$1.29 \times 10^{-1}$
	25L	$6.52 \times 10^{-2}$		$1.30 \times 10^{-2}$		$6.52 \times 10^{-2}$	$1.30 \times 10^{-2}$	$1.29 \times 10^{-1}$	$1.29 \times 10^{-1}$
	30	$7.07 \times 10^{-2}$		$1.36 \times 10^{-2}$		$7.07 \times 10^{-2}$	$1.36 \times 10^{-2}$	$1.02 \times 10^{-1}$	$1.02 \times 10^{-1}$
	30L	$5.54 \times 10^{-2}$		$1.12 \times 10^{-2}$		$5.54 \times 10^{-2}$	$1.12 \times 10^{-2}$	$1.02 \times 10^{-1}$	$1.02 \times 10^{-1}$
	35	$6.45 \times 10^{-2}$		$1.29 \times 10^{-2}$		$6.45 \times 10^{-2}$	$1.29 \times 10^{-2}$	$8.29 \times 10^{-2}$	$8.29 \times 10^{-2}$
	35L	$5.00 \times 10^{-2}$		$1.05 \times 10^{-2}$		$5.00 \times 10^{-2}$	$1.05 \times 10^{-2}$	$8.29 \times 10^{-2}$	$8.29 \times 10^{-2}$
	45	$5.16 \times 10^{-2}$		$1.05 \times 10^{-2}$		$5.16 \times 10^{-2}$	$1.05 \times 10^{-2}$	$6.52 \times 10^{-2}$	$6.52 \times 10^{-2}$
	45L	$4.00 \times 10^{-2}$		$8.50 \times 10^{-3}$		$4.00 \times 10^{-2}$	$8.50 \times 10^{-3}$	$6.52 \times 10^{-2}$	$6.52 \times 10^{-2}$
	55	$4.17 \times 10^{-2}$		$8.74 \times 10^{-3}$		$4.17 \times 10^{-2}$	$8.74 \times 10^{-3}$	$5.39 \times 10^{-2}$	$5.39 \times 10^{-2}$
	55L	$3.14 \times 10^{-2}$		$6.85 \times 10^{-3}$		$3.14 \times 10^{-2}$	$6.85 \times 10^{-3}$	$5.39 \times 10^{-2}$	$5.39 \times 10^{-2}$
	65	$3.08 \times 10^{-2}$		$6.56 \times 10^{-3}$		$3.08 \times 10^{-2}$	$6.56 \times 10^{-3}$	$4.62 \times 10^{-2}$	$4.62 \times 10^{-2}$
	65L	$2.36 \times 10^{-2}$		$5.15 \times 10^{-3}$		$2.36 \times 10^{-2}$	$5.15 \times 10^{-3}$	$4.62 \times 10^{-2}$	$4.62 \times 10^{-2}$

 $K_{AR1}$  : Equivalent factor in the  $M_a$  radial direction when one LM block is used $K_{AL1}$  : Equivalent factor in the  $M_a$  reverse-radial direction when one LM block is used $K_{AR2}$  : Equivalent factor in the  $M_a$  radial direction when two

LM blocks are used in close contact with each other

 $K_{AL2}$  : Equivalent factor in the  $M_a$  reverse-radial direction when two LM blocks are used in close contact with each other $K_{B1}$  :  $M_b$  Equivalent factor when one LM block is used $K_{B2}$  :  $M_b$  Equivalent factor when two LM blocks are used in close contact with each other $K_{CR}$  : Equivalent factor in the  $M_c$  radial direction $K_{CL}$  : Equivalent factor in the  $M_c$  reverse-radial direction

## Double-Axis Use

### ● Determining the Operating Conditions

Set the conditions needed to calculate the applied load and service life in hours for the LM System.

- (1) Mass:  $m$  (kg)
- (2) Direction of the working load
- (3) Position of the working point (e.g., center of gravity):  $l_2, l_3, h_1$  (mm)
- (4) Thrust position:  $l_4, h_2$  (mm)
- (5) LM system arrangement:  $l_0, l_1$  (mm)  
(No. of units and axes)
- (6) Velocity diagram  
Speed:  $V$  (mm/s)  
Time constant:  $t_n$  (s)  
Acceleration:  $\alpha_n$  (mm/s<sup>2</sup>)

$$(\alpha_n = \frac{V}{t_n})$$

- (7) Duty cycle  
Number of reciprocations per minute:  $N_1$  (min<sup>-1</sup>)
  - (8) Stroke length:  $l_s$  (mm)
  - (9) Average speed:  $V_m$  (m/s)
  - (10) Required service life in hours:  $L_h$  (h)
- Gravitational acceleration  $g = 9.8$  (m/s<sup>2</sup>)

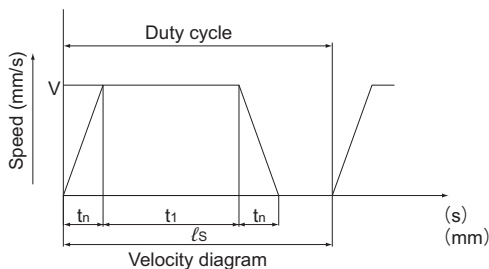
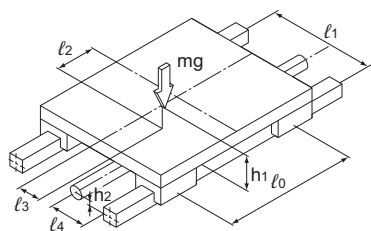


Fig. 6: Operating Conditions

### ● Applied Load Equation

The load applied to the LM Guide varies with external forces such as the location of the center of gravity of the load, the position of the thrust, inertia generated by acceleration and deceleration during starts and stops, and cutting resistance.

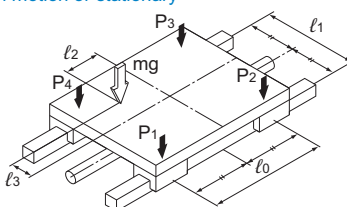
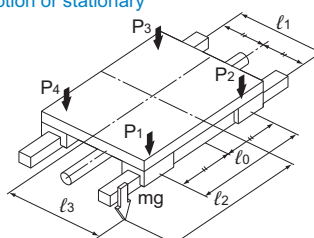
In selecting an LM Guide, it is necessary to obtain the value of the applied load while taking into account these conditions.

Calculate the load applied to the LM Guide in each of the examples 1 to 10 shown below.

$m$	: Mass	(kg)
$l_n$	: Distance	(mm)
$F_n$	: External force	(N)
$P_n$	: Applied load (radial/reverse-radial direction)	(N)
$P_{nT}$	: Applied load (lateral directions)	(N)
$g$	: Gravitational acceleration	(m/s <sup>2</sup> )
	( $g = 9.8 \text{ m/s}^2$ )	
$V$	: Speed	(m/s)
$t_n$	: Time constant	(s)
$\alpha_n$	: Acceleration	(m/s <sup>2</sup> )

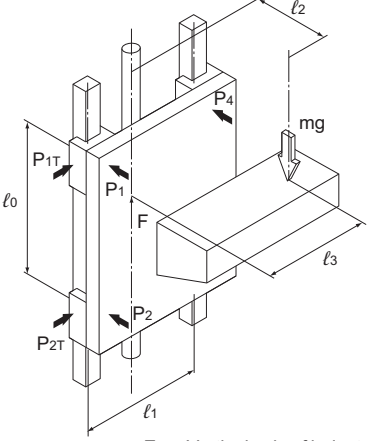
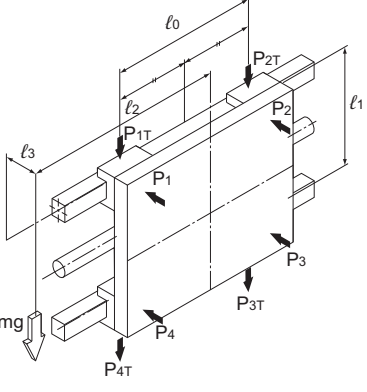
$$(\alpha_n = \frac{V}{t_n})$$

### Example

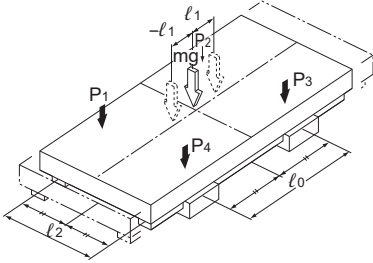
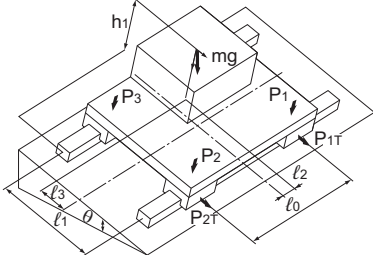
	Operating conditions	Applied load equation
1	Horizontal mount (with the block moving) Uniform motion or stationary 	$P_1 = \frac{mg}{4} + \frac{mg \cdot l_2}{2 \cdot l_0} - \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_2 = \frac{mg}{4} - \frac{mg \cdot l_2}{2 \cdot l_0} - \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_3 = \frac{mg}{4} - \frac{mg \cdot l_2}{2 \cdot l_0} + \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_4 = \frac{mg}{4} + \frac{mg \cdot l_2}{2 \cdot l_0} + \frac{mg \cdot l_3}{2 \cdot l_1}$
2	Horizontal mount, overhung (with the block moving) Uniform motion or stationary 	$P_1 = \frac{mg}{4} + \frac{mg \cdot l_2}{2 \cdot l_0} + \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_2 = \frac{mg}{4} - \frac{mg \cdot l_2}{2 \cdot l_0} + \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_3 = \frac{mg}{4} - \frac{mg \cdot l_2}{2 \cdot l_0} - \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_4 = \frac{mg}{4} + \frac{mg \cdot l_2}{2 \cdot l_0} - \frac{mg \cdot l_3}{2 \cdot l_1}$

Note) Load is positive in the direction of the arrow.

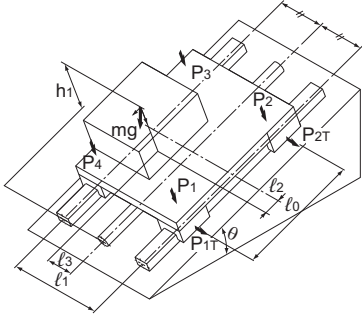
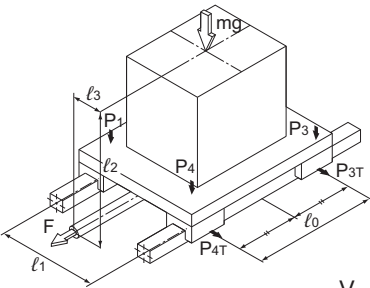


	Operating conditions	Applied load equation
3	<p><b>Vertical mount</b> <b>Uniform motion or stationary</b></p>  <p>E.g.: Vertical axis of industrial robot, automatic coating machine, lifter</p>	$P_1 = P_4 = - \frac{mg \cdot l_2}{2 \cdot l_0}$ $P_2 = P_3 = \frac{mg \cdot l_2}{2 \cdot l_0}$ $P_{1T} = P_{4T} = \frac{mg \cdot l_3}{2 \cdot l_0}$ $P_{2T} = P_{3T} = - \frac{mg \cdot l_3}{2 \cdot l_0}$
4	<p><b>Wall mount</b> <b>Uniform motion or stationary</b></p>  <p>E.g.: Travel axis of cross-rail loader</p>	$P_1 = P_2 = - \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_3 = P_4 = \frac{mg \cdot l_3}{2 \cdot l_1}$ $P_{1T} = P_{4T} = \frac{mg}{4} + \frac{mg \cdot l_2}{2 \cdot l_0}$ $P_{2T} = P_{3T} = \frac{mg}{4} - \frac{mg \cdot l_2}{2 \cdot l_0}$

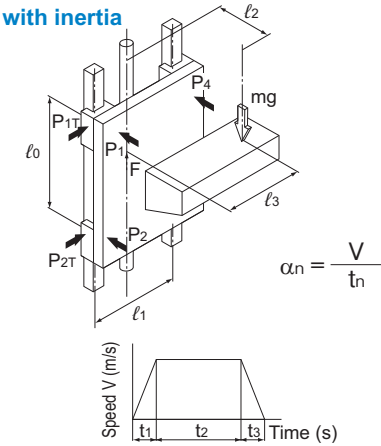
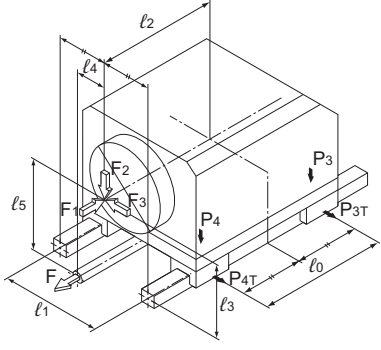
Note) Load is positive in the direction of the arrow.

	Operating conditions	Applied load equation
5	<p><b>With the LM rails moving</b> <b>Horizontal mount</b></p>  <p>E.g.: XY table sliding fork</p>	$P_1 \text{ to } P_4 (\text{max}) = \frac{mg}{4} + \frac{mg \cdot l_1}{2 \cdot l_0}$ $P_1 \text{ to } P_4 (\text{min}) = \frac{mg}{4} - \frac{mg \cdot l_1}{2 \cdot l_0}$
6	<p><b>Lateral tilt mount</b></p>  <p>E.g.: NC lathe carriage</p>	$P_1 = + \frac{mg \cdot \cos \theta}{4} + \frac{mg \cdot \cos \theta \cdot l_2}{2 \cdot l_0}$ $- \frac{mg \cdot \cos \theta \cdot l_3}{2 \cdot l_1} + \frac{mg \cdot \sin \theta \cdot h_1}{2 \cdot l_1}$ $P_{1T} = \frac{mg \cdot \sin \theta}{4} + \frac{mg \cdot \sin \theta \cdot l_2}{2 \cdot l_0}$ $P_2 = + \frac{mg \cdot \cos \theta}{4} - \frac{mg \cdot \cos \theta \cdot l_2}{2 \cdot l_0}$ $- \frac{mg \cdot \cos \theta \cdot l_3}{2 \cdot l_1} + \frac{mg \cdot \sin \theta \cdot h_1}{2 \cdot l_1}$ $P_{2T} = \frac{mg \cdot \sin \theta}{4} - \frac{mg \cdot \sin \theta \cdot l_2}{2 \cdot l_0}$ $P_3 = + \frac{mg \cdot \cos \theta}{4} - \frac{mg \cdot \cos \theta \cdot l_2}{2 \cdot l_0}$ $+ \frac{mg \cdot \cos \theta \cdot l_3}{2 \cdot l_1} - \frac{mg \cdot \sin \theta \cdot h_1}{2 \cdot l_1}$ $P_{3T} = \frac{mg \cdot \sin \theta}{4} - \frac{mg \cdot \sin \theta \cdot l_2}{2 \cdot l_0}$ $P_4 = + \frac{mg \cdot \cos \theta}{4} + \frac{mg \cdot \cos \theta \cdot l_2}{2 \cdot l_0}$ $+ \frac{mg \cdot \cos \theta \cdot l_3}{2 \cdot l_1} - \frac{mg \cdot \sin \theta \cdot h_1}{2 \cdot l_1}$ $P_{4T} = \frac{mg \cdot \sin \theta}{4} + \frac{mg \cdot \sin \theta \cdot l_2}{2 \cdot l_0}$

Note) Load is positive in the direction of the arrow.

	Operating conditions	Applied load equation
7	<p><b>Longitudinal tilt mount</b></p>  <p>E.g.: NC lathe tool rest</p>	$P_1 = + \frac{mg \cdot \cos\theta}{4} + \frac{mg \cdot \cos\theta \cdot \ell_2}{2 \cdot \ell_0}$ $- \frac{mg \cdot \cos\theta \cdot \ell_3}{2 \cdot \ell_1} + \frac{mg \cdot \sin\theta \cdot h_1}{2 \cdot \ell_0}$ $P_{1T} = + \frac{mg \cdot \sin\theta \cdot \ell_3}{2 \cdot \ell_0}$ $P_2 = + \frac{mg \cdot \cos\theta}{4} - \frac{mg \cdot \cos\theta \cdot \ell_2}{2 \cdot \ell_0}$ $- \frac{mg \cdot \cos\theta \cdot \ell_3}{2 \cdot \ell_1} - \frac{mg \cdot \sin\theta \cdot h_1}{2 \cdot \ell_0}$ $P_{2T} = - \frac{mg \cdot \sin\theta \cdot \ell_3}{2 \cdot \ell_0}$ $P_3 = + \frac{mg \cdot \cos\theta}{4} - \frac{mg \cdot \cos\theta \cdot \ell_2}{2 \cdot \ell_0}$ $+ \frac{mg \cdot \cos\theta \cdot \ell_3}{2 \cdot \ell_1} - \frac{mg \cdot \sin\theta \cdot h_1}{2 \cdot \ell_0}$ $P_{3T} = - \frac{mg \cdot \sin\theta \cdot \ell_3}{2 \cdot \ell_0}$ $P_4 = + \frac{mg \cdot \cos\theta}{4} + \frac{mg \cdot \cos\theta \cdot \ell_2}{2 \cdot \ell_0}$ $+ \frac{mg \cdot \cos\theta \cdot \ell_3}{2 \cdot \ell_1} + \frac{mg \cdot \sin\theta \cdot h_1}{2 \cdot \ell_0}$ $P_{4T} = + \frac{mg \cdot \sin\theta \cdot \ell_3}{2 \cdot \ell_0}$
8	<p><b>Horizontal mount with inertia</b></p>  <p>E.g.: Conveyance truck</p>	<p>During acceleration</p> $P_1 = P_4 = \frac{mg}{4} - \frac{m \cdot \alpha_1 \cdot \ell_2}{2 \cdot \ell_0}$ $P_2 = P_3 = \frac{mg}{4} + \frac{m \cdot \alpha_1 \cdot \ell_2}{2 \cdot \ell_0}$ $P_{1T} = P_{4T} = \frac{m \cdot \alpha_1 \cdot \ell_3}{2 \cdot \ell_0}$ $P_{2T} = P_{3T} = - \frac{m \cdot \alpha_1 \cdot \ell_3}{2 \cdot \ell_0}$ <p>During uniform motion</p> $P_1 \text{ to } P_4 = \frac{mg}{4}$ <p>During deceleration</p> $P_1 = P_4 = \frac{mg}{4} + \frac{m \cdot \alpha_3 \cdot \ell_2}{2 \cdot \ell_0}$ $P_2 = P_3 = \frac{mg}{4} - \frac{m \cdot \alpha_3 \cdot \ell_2}{2 \cdot \ell_0}$ $P_{1T} = P_{4T} = - \frac{m \cdot \alpha_3 \cdot \ell_3}{2 \cdot \ell_0}$ $P_{2T} = P_{3T} = \frac{m \cdot \alpha_3 \cdot \ell_3}{2 \cdot \ell_0}$

Note) Load is positive in the direction of the arrow.

	Operating conditions	Applied load equation
9	<p><b>Vertical mount with inertia</b></p>  <p style="text-align: center;"><math>\alpha_n = \frac{V}{t_n}</math></p> <p style="text-align: center;">Velocity diagram E.g.: Conveyance lift</p>	<p>During acceleration</p> $P_1 = P_4 = - \frac{m(g + \alpha_1) l_2}{2 \cdot l_0}$ $P_2 = P_3 = \frac{m(g + \alpha_1) l_2}{2 \cdot l_0}$ $P_{1T} = P_{4T} = \frac{m(g + \alpha_1) l_3}{2 \cdot l_0}$ $P_{2T} = P_{3T} = - \frac{m(g + \alpha_1) l_3}{2 \cdot l_0}$ <p>During uniform motion</p> $P_1 = P_4 = - \frac{mg \cdot l_2}{2 \cdot l_0}$ $P_2 = P_3 = \frac{mg \cdot l_2}{2 \cdot l_0}$ $P_{1T} = P_{4T} = \frac{mg \cdot l_3}{2 \cdot l_0}$ $P_{2T} = P_{3T} = - \frac{mg \cdot l_3}{2 \cdot l_0}$ <p>During deceleration</p> $P_1 = P_4 = - \frac{m(g - \alpha_3) l_2}{2 \cdot l_0}$ $P_2 = P_3 = \frac{m(g - \alpha_3) l_2}{2 \cdot l_0}$ $P_{1T} = P_{4T} = \frac{m(g - \alpha_3) l_3}{2 \cdot l_0}$ $P_{2T} = P_{3T} = - \frac{m(g - \alpha_3) l_3}{2 \cdot l_0}$
10	<p><b>Horizontal mount with external force</b></p>  <p style="text-align: center;">E.g.: Drill unit, milling machine, lathe, machining center, and other cutting machines</p>	<p>Under force <math>F_1</math></p> $P_1 = P_4 = - \frac{F_1 \cdot l_5}{2 \cdot l_0}$ $P_2 = P_3 = \frac{F_1 \cdot l_5}{2 \cdot l_0}$ $P_{1T} = P_{4T} = \frac{F_1 \cdot l_4}{2 \cdot l_0}$ $P_{2T} = P_{3T} = - \frac{F_1 \cdot l_4}{2 \cdot l_0}$ <p>Under force <math>F_2</math></p> $P_1 = P_4 = \frac{F_2}{4} + \frac{F_2 \cdot l_2}{2 \cdot l_0}$ $P_2 = P_3 = \frac{F_2}{4} - \frac{F_2 \cdot l_2}{2 \cdot l_0}$ <p>Under force <math>F_3</math></p> $P_1 = P_2 = \frac{F_3 \cdot l_3}{2 \cdot l_1}$ $P_3 = P_4 = - \frac{F_3 \cdot l_3}{2 \cdot l_1}$ $P_{1T} = P_{4T} = - \frac{F_3}{4} - \frac{F_3 \cdot l_2}{2 \cdot l_0}$ $P_{2T} = P_{3T} = - \frac{F_3}{4} + \frac{F_3 \cdot l_2}{2 \cdot l_0}$

Note) Load is positive in the direction of the arrow.